HTGR Technology Course for the Nuclear Regulatory Commission

May 24 – 27, 2010

Module 8
Fuel Performance

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General Atomics





Outline



- Fuel operating experience in HTGRs
- Fuel irradiation and post-irradiation examination (PIE)
- Safety criteria and performance limits
- Fuel performance modeling
- Fuel cycle issues

Reactor Operation Experience for Fuel Has Been Good

- Four experimental and three power reactors using coated particles
 - UK, US, Germany, Japan, China
- Commercial-scale production and reactor operation (and supporting R&D) have lead to
 - Understanding of fabrication
 - Understanding of irradiation behavior and limits
 - Fuel quality and performance improvements

....coated particles w/~50,000 kg HM fabricated





Coated Particle Fuel Has Been Used Internationally In Seven Gas-Cooled Reactors

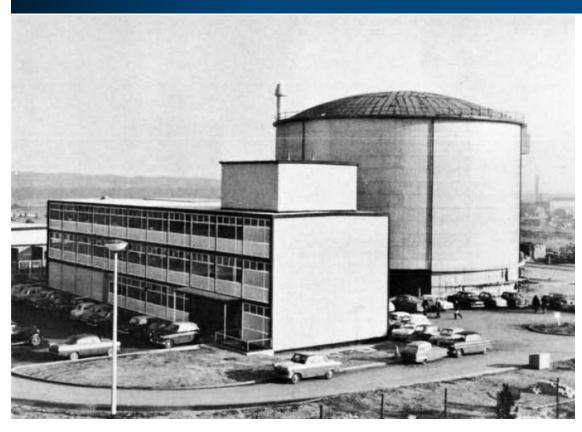
	Fuel	Fuel Enrichment (%)	Maximum			Assaurana	Dawaria	
Reactor			Temp (°C)	Burnup (% fima)	Fast neutron fluence (10 ²⁵ n/m ²)	Average Power Density (w/cc)*	Power/p article (milliwatt /part)	Packing Fraction (%)*
Typical Pebble Bed	TRISO (UO ₂)	7.8	1048	8.75	2.4	10	55	7
Typical Prismatic	TRISO (UCO)	14 or 20	1250	26	4.5	31	40	23
Dragon	BISO/TRISO Various							
Peach Bottom I	BISO (U/Th)C ₂	93	1400	28		28		
AVR	BISO/TRISO Various	93	1100- >1280	16		7		40
THTR	BISO (U/Th)O ₂	93	1100	10	4	17	40	40
Fort. St. Vrain	TRISO (U/Th)C ₂ , ThC ₂	93	1200	16	4	29		60
HTTR	TRISO UO ₂	3 to 10 (6 ave)	1490	~1	<1	24	35	28
HTR-10	TRISO UO ₂	17	1200	~1	<1	6		35

Power density in volume where there are coated particles (compact and fueled region of pebble)

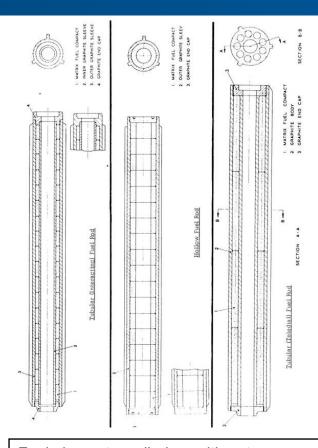




Dragon, Winfrith, Dorset, UK



Operated 1965 to 1976 developing many new fuel designs – Tested BISO and TRISO with many fuel forms including Pu fuels – important early fuel developments were almost all made at Dragon



Fuel element – cylinders with outer sleeve, annular compacts, inner graphite filler, some elements internal purge sweeps fission products to monitoring and trapping system

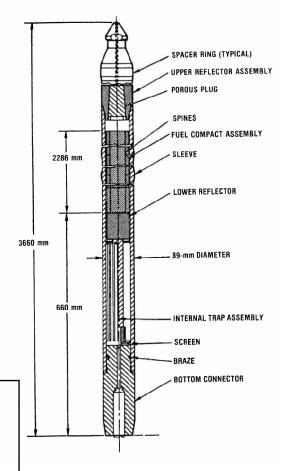


Peach Bottom I (40 MWe), Delta, Pennsylvania



- Used BISO (U/Th)C₂ fuel particles no longer proposed for use in HTGRs
- First core experienced failures
- Corrected in the second core

Fuel element – cylinders with outer sleeve, annular compacts, inner graphite filler, internal purged sweeps fission products to trapping system

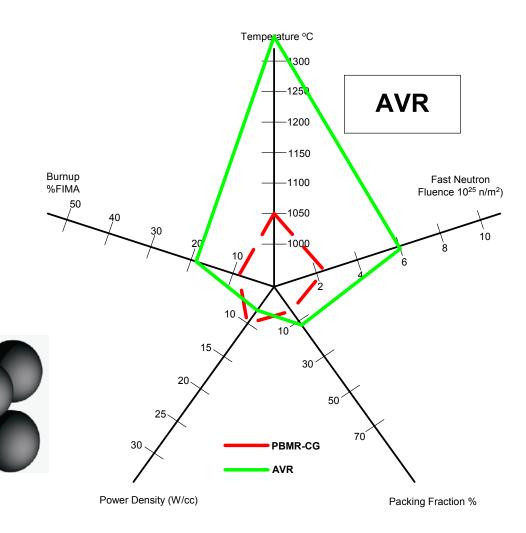




AVR (Arbeitsgemeinshaft Versuchsreactor), Hanau, Germany

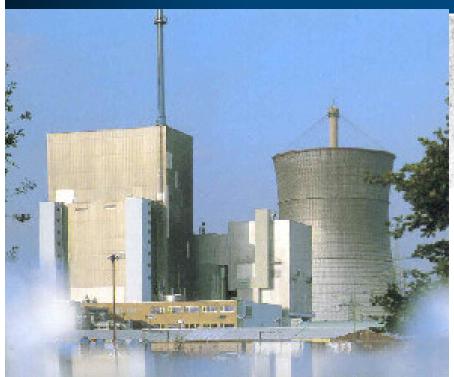


BISO and TRISO pebble fuels of various qualities tested over 21 years – total of 2 million pebbles
Operated with hot helium temperature up to 950 °C





THTR (Thorium High Temperature Reactor), Hamm-Uentrop, Germany



Temperature °C -1300 -1250 **THTR** -1200-1150 Burnup Fast Neutron %FIMA Fluence 10²⁵ n/m²) PBMR-CG **THTR** Power Density (W/cc) Packing Fraction %

BISO (U/Th)O₂ fuels tested during 5 (1983 – 1988) year operation Power reactor operated on the power grid – steam cycle with 750 °C hot helium - ~1million spheres





HTR-10, Beijing, China

Burnup

%FIMA



1250 HTR-10

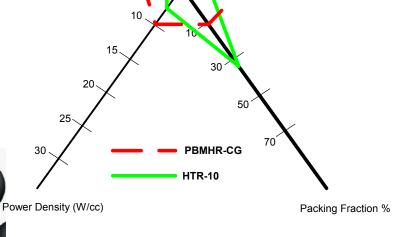
Temperature °C

1300

Operating with TRISO UO₂ pebble fuel since 2003

27,000 spheres

Small experimental reactor bring technology to China

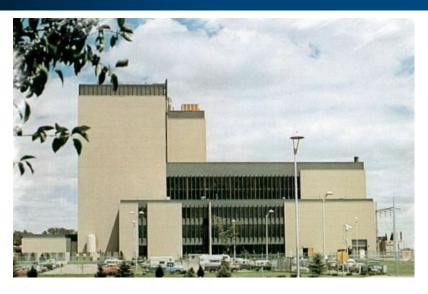




Fast Neutron

Fluence 10²⁵ n/m²)

Fort St. Vrain, Platteville, Colorado

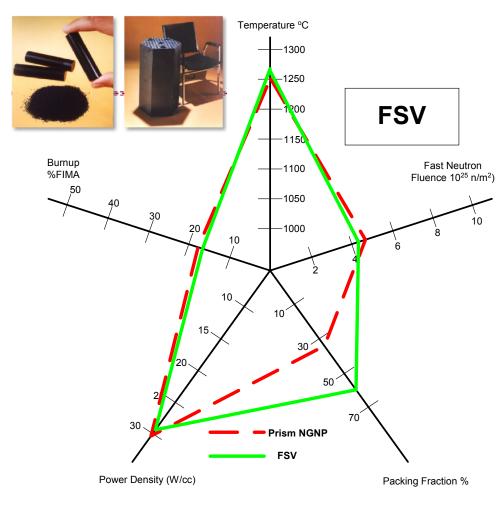


Operated on power grid for ~13 years (1976-1989) –reduced power

TRISO (U/Th)C₂ fissile and ThC₂ fertile fuel

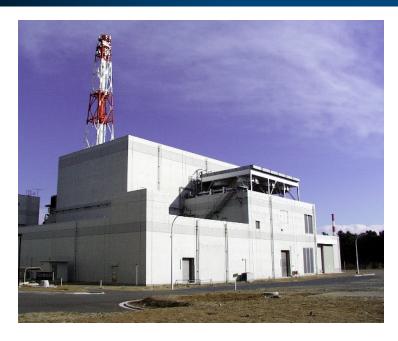
2450 fuel assemblies, 7.5 million compacts, 33,000 kg HM in fuel

Fuel performed well





HTTR (High Temperature Engineering Test Reactor), Oarai, Japan



HTTR Fast Neutron Fluence 10²⁵ n/m²)

Power Density (W/cc)

Currently operating with first core TRISO UO₂ fuel to 2014

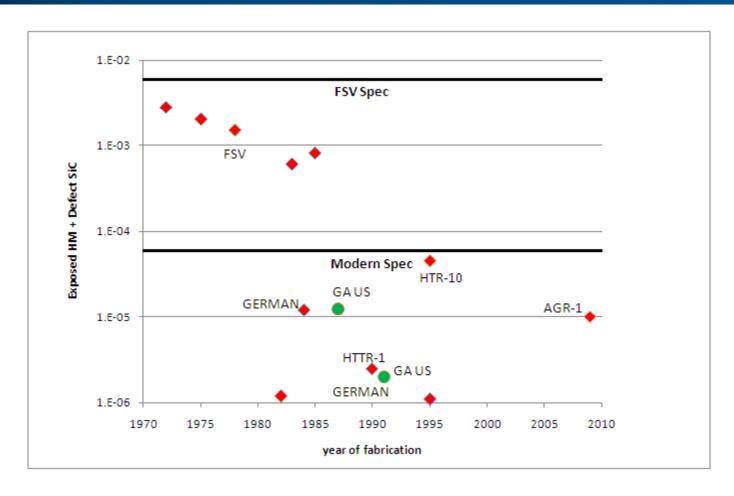
Operating with 950°C helium temperature

Excellent fuel performance – low measured fission gas release



Packing Fraction %

Improved Equipment and Fabrication Procedures Provided Substantial as-Manufactured Quality Improvement

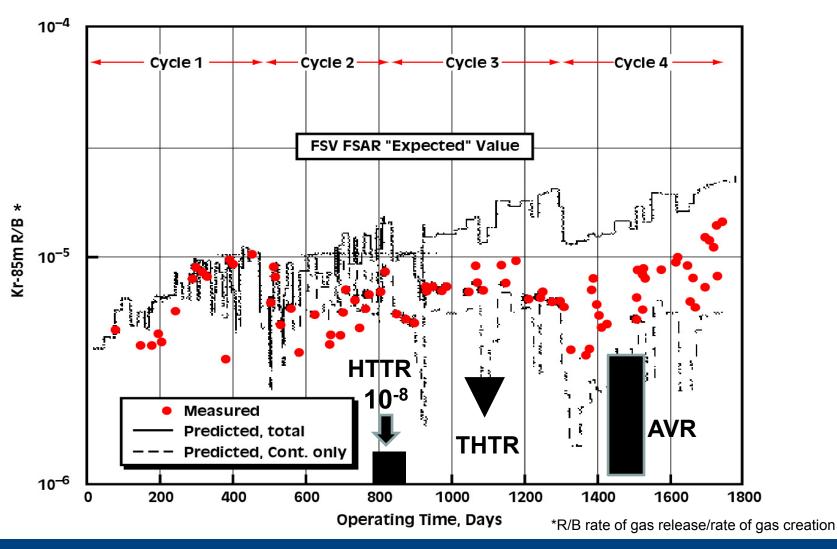


But some fuel has not performed well under irradiation





In-Pile ^{85m}Kr Release Measurements in FSV Indicate Good Coated Particle Fuel Performance







Outline

Fuel operating experience in HTGRs



- Fuel irradiation and post-irradiation examination (PIE)
- Safety criteria and performance limits
- Fuel performance modeling
- Fuel cycle issues

CP Irradiation & PIE Procedures and Equipment are Well-Developed Tools for Understanding CP Fuel

Fuel irradiations

- Test units compacts, pebbles, particles
- Test reactors and test equipment
- Irradiations are conducted to
 - Determine fission product barrier failure mechanisms, rates, limitations, and margins
 - Design information on irradiated fuel materials
 - Demonstrate performance of evolving fuel developments
 - Validate fuel performance and fission product transport methods
- Irradiation test measurements
 - Temperatures, neutron spectra and fluence, fission gas release

Post-irradiation examinations (PIE)

- PIE facilities and equipment extract quantitative data
- Results contribute to understanding and quantification of fuel performance





Irradiation Facilities at INL – ORNL & Worldwide



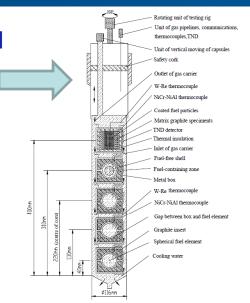
Many other reactors have been used for Coated Particle Irradiations

Advanced
Test Reactor
INL

High Flux Isotope Reactor - ORNL

High Flux Reactor Petten, Netherlands

Russia: IVV-2M
Pebbles
SM-3/RBT-6
Compacts

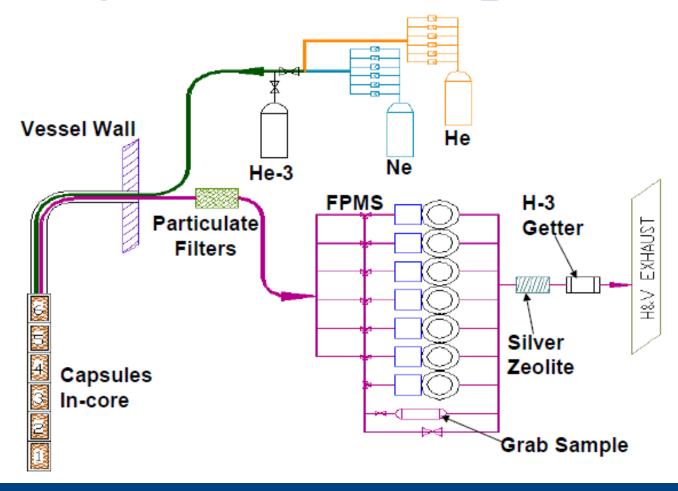






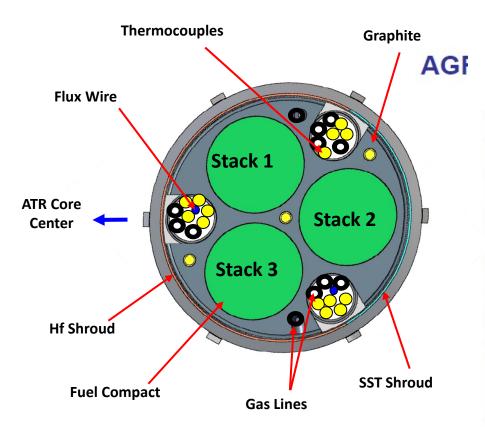
Irradiation Facilities Measure Irradiation Conditions and Coating Integrity via in-Reactor Fission Gas Release

AGR-1 Experiment Block Diagram



Six (6)-Capsule Test Train Design for AGR-1

Individual Cell Features



AGR-1 test train assembly 6-individual instrumented capsules



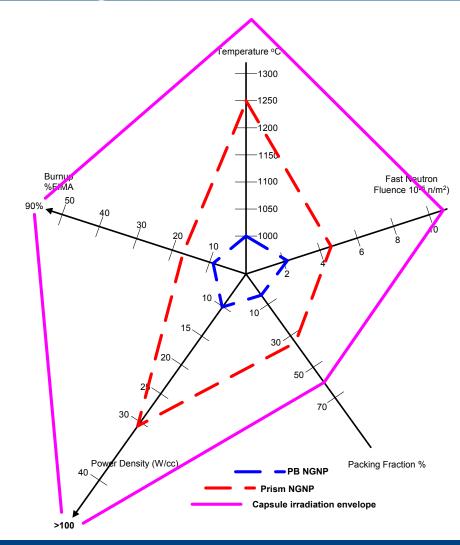
Twelve, 0.5" diam, 1" long compacts/cell



Capsule Irradiations Envelope Far Exceeded NGNP Operating Envelopes

All Coated Particle Irradiations

- Earlier irradiations most Coatings survived
- But performance did not meet modern standards in all cases
 - 1400°C
 - 12 x 10²⁵ n/m²
 - 60% PF
 - 100 w/cc (fuel region)
 - •~90% FIMA





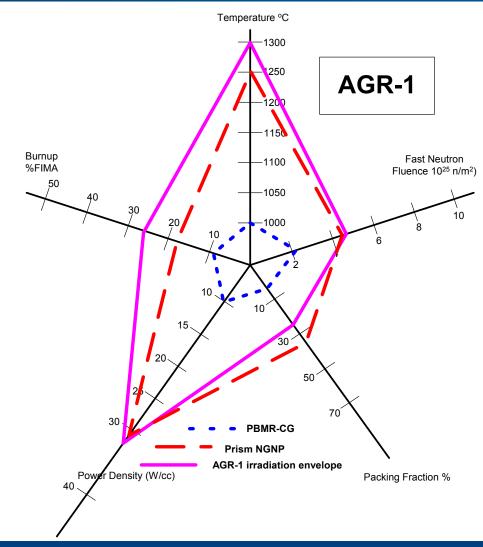


AGR-1 Irradiation Conditions Closely Match Expected Prismatic NGNP Service Conditions

And satisfied performance requirements

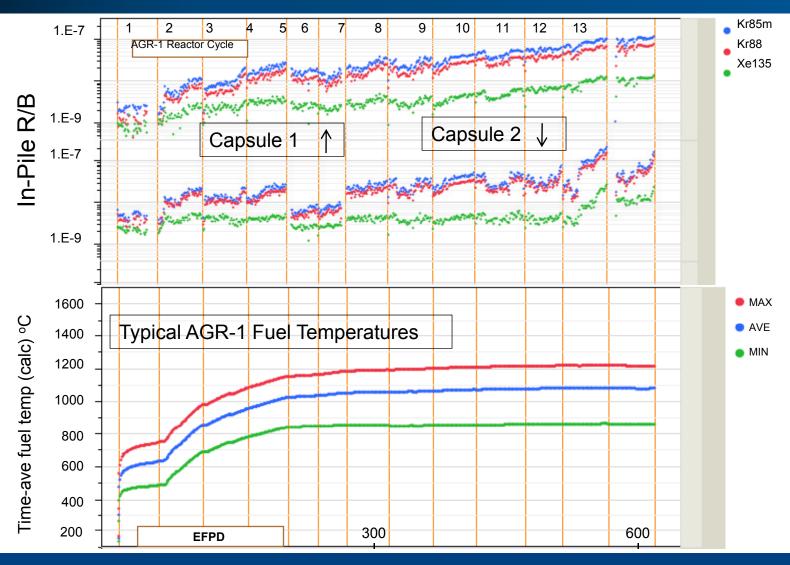
(based on in-pile fission gas release measurements)

- •1300°C
- 4.5 x 10²⁵ n/m²
- 28% PF
- 32 w/cc (fuel region)
- ~26% FIMA





Outstanding Coated-Particle Fuel Performance Observed in Most Recent US Irradiation







Summary – Fuel Irradiations

TRISO - extensive irradiation testing

- Exceeding NGNP operating envelope
- German (pebble) and recent US (compact) irradiations demonstrate required performance

Additional testing needed

- Establish repeatability statistical confidence
- Fuel fabricated on production-scale equipment
- Obtain additional design data, limitations, margins
- Validate fuel and fission product design methods





Techniques for Coated Particle PIE are Well Developed



ORNL

INL

Coated particle post-irradiation examinations performed at well-equipped hot cells, TRIGA reactor, accident testing facilities at:

- Oak Ridge National Lab
- Idaho National Lab









Specialized Methods Have Been Developed for Coated Particle Fuel Examination

Examine irradiated compacts and pebbles

- Dimensions, visual, metallographic, thermal/mechanical properties
- Fission gas release (R/B) reactivation
- Solid fission product release
- Accident behavior

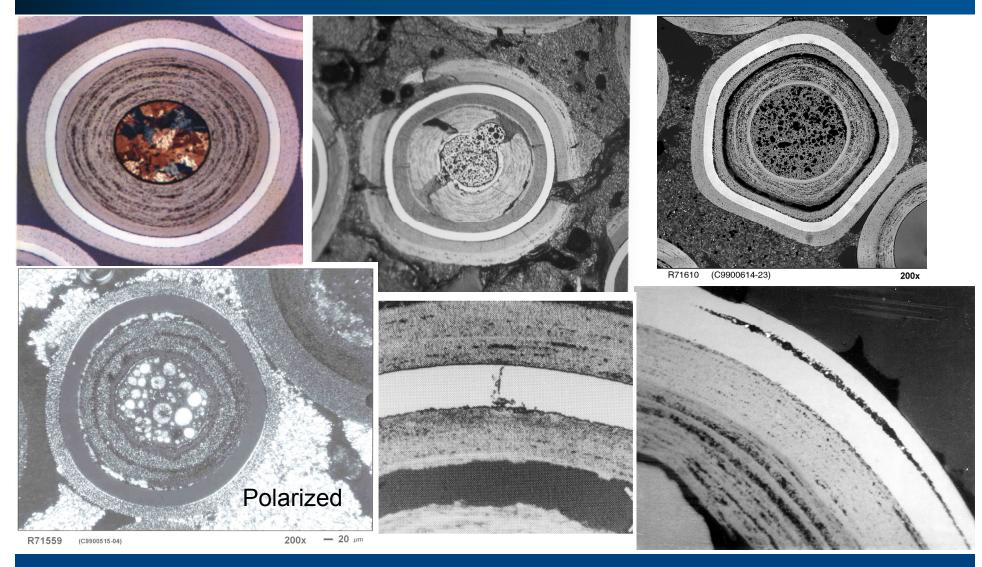
Examine irradiated individual particles

- Compact & pebble deconsolidation
- Individual microsphere gamma analyses (IMGA)
- Exposed or uncoated heavy metal
- Metallography
- Scanning electron microscope/microprobe





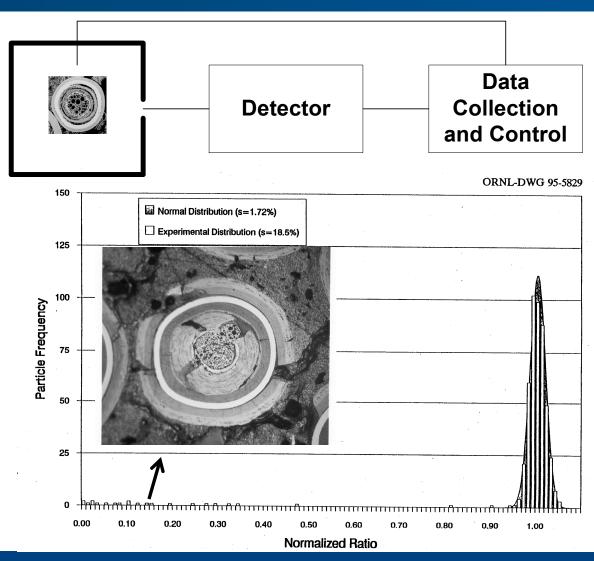
Metallography Reveals Condition of Particles w/SEM –Microprobe –Distribution of Elements (variety of irradiations)





Individual Particles Can be Gamma-Counted and Isolated for Examination

- IMGA gamma counts a large number of individual particles and tallies results
- Automated handling & counting
- Pick out problem particles for detailed examination

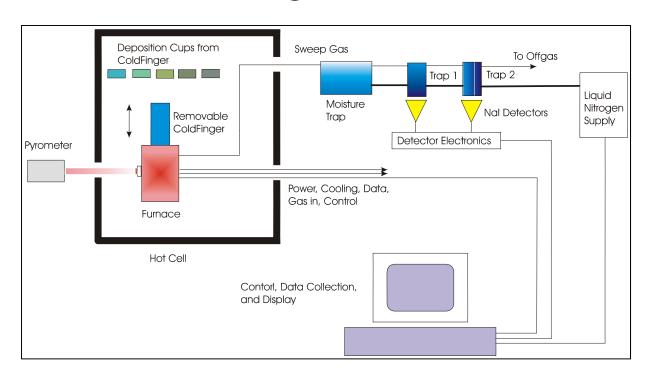


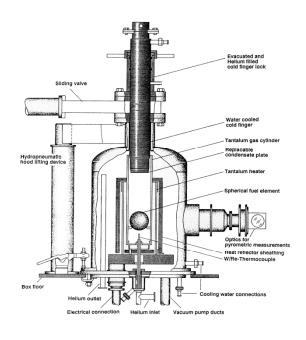




Accident Testing of Irradiated Fuel

Furnace configuration



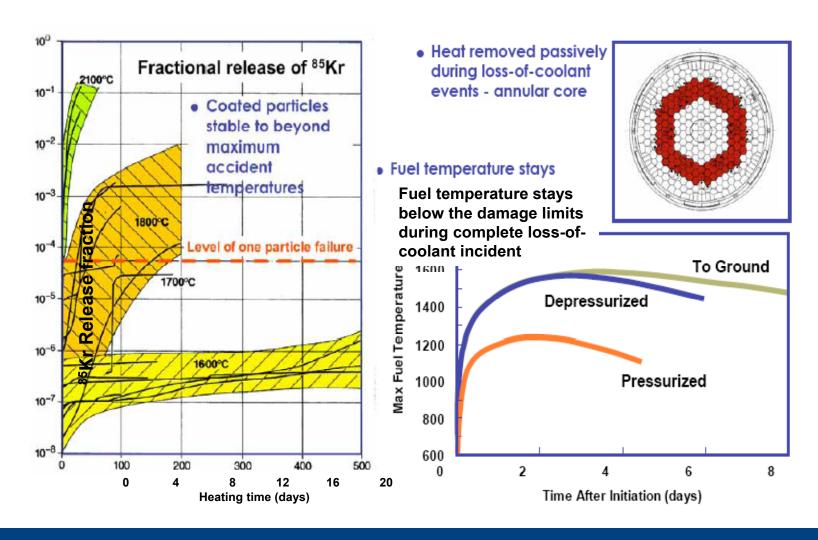


Test Compacts, Spheres, Particles (ORNL, INL, Worldwide)





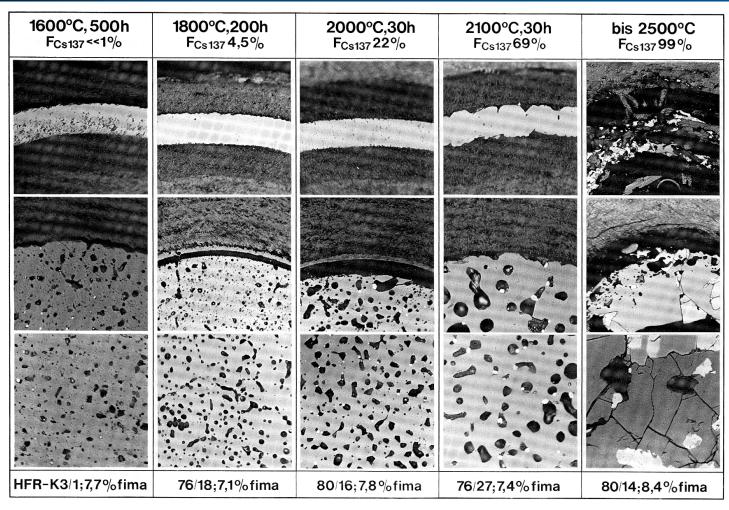
FG Data Indicates Coating Failure Initiated above 1600 °C Satisfying the Accident Criterion is Achieved by Reactor Design







PIE Reveals Details of Coating Response to Accident Conditions – Determine Mechanisms & Rates



SiC Coating

Kernelbuffer interface

Kernel

Ceramographic sections through UO₂ TRISO particles



Summary – Post Irradiation Examination

- Irradiation testing of CP fuels can realistically simulate reactor conditions
- Irradiation facilities can measure and control irradiation conditions and collect in-pile data
- Specialized PIE tools have been developed for coated particle fuel to obtain quantitative performance and design data
- Accident conditions can be simulated and data on fission product barriers and fission product release collected



Outline

- Fuel operating experience in HTGRs
- Fuel irradiation and post-irradiation examination (PIE)



- Safety criteria and performance limits
- Fuel performance modeling
- Fuel cycle issues



Fuel Safety Approach

- Fuel safety criteria are related to the fuel fission product barriers – coatings
- Based on meeting plant top-level dose limits with margin
- Coating failure allowance allocated to as-manufactured and in-service performance
- Testing established service environment where performance requirements are achieved
- Coating integrity during operation is protected by Operational Technical Specifications
 - Parameters are monitored and limited to meet safety criteria and stay within performance limits
 - Coating integrity monitored by primary coolant radioactivity
- Coating failure limitation during accidents is achieved by reactor design – passive, conductive heat loss





Estimated Maximum Service Conditions for Pebble & Prismatic NGNP Fuel (not Limits)

Parameter	Maximum Value*	Maximum Value*	
	(PBMR-CG)	(Prismatic NGNP)	
Maximum fuel temperature–normal operation,	1048	1400	
°C			
Maximum time averaged fuel temperature, °C	1048	1250	
Fuel temperature (accident conditions), °C	1483	1600	
Fuel burnup, % FIMA	8.75	17**	
Fast neutron fluence, 10^{25} n/m ² (E > 0.18 MeV)	4	5	

^{*}Anticipated max. temperatures are <u>not</u> design limits. These temperatures may be exceeded for a limited time (days or weeks) without resulting in fuel failure and can be exceeded by a small fraction of the fuel for longer periods without resulting in excessive fission product release.

^{**}Estimated FIMA for 14% enriched reference fuel particle under development by NGNP/AGR Fuel Program





^{*}These do not represent "cliffs" where if exceeded failure will result

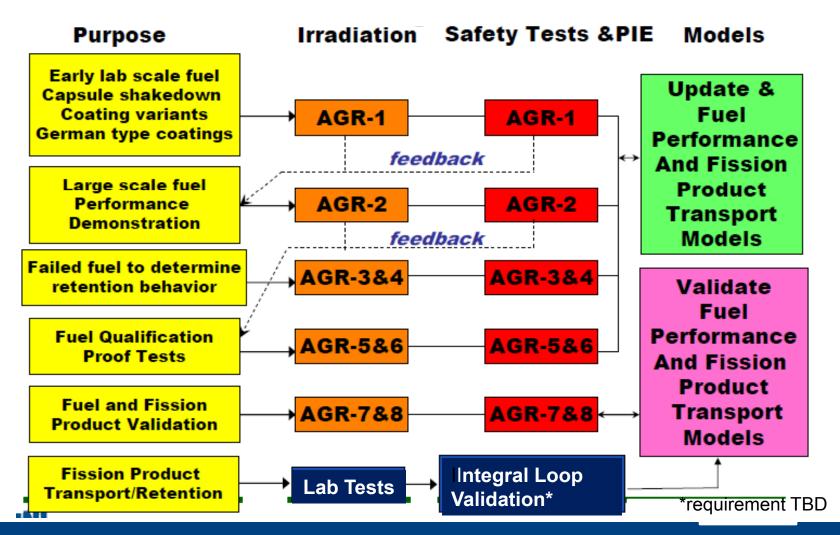
Comprehensive Fuel Qualification Program Being Conducted by NGNP/AGR Fuel Program

- Process development
- Test sample fabrication
- Irradiation testing & PIE
- Accident testing
- Validate fuel performance models
- Fuel product and process specifications
- Technology for commercial fuel fabrication
- Reduce market risk
- Qualify fuel for NGNP





NGNP/AGR Fuel Program Overview





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- Fuel operating experience in HTGRs
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- Safety criteria and performance limits



- Fuel performance modeling
- Fuel cycle issues

Role of Fuel Performance Modeling

- Guide current and future particle designs
- Assist in irradiation and safety experiment planning
- Predict observed fuel failures
- Predict fission product transport through particles and matrix
- Interpolate fuel performance for core design assessments

.....INL leading US model development - PARFUME





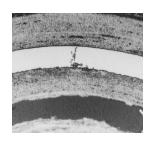
Coating Failure Mechanisms to be Modeled





- Internal gas pressure
- Irradiation induced dimensional changes
- Interactions between coatings
- Fuel kernel thermo-chemistry
 - Oxygen management
 - Fission product compounds and phases
- Carbon Transport in temperature gradient
 - Kernel migration
- Chemical reactions with coating
 - CO/CO₂, palladium, lanthanides, impurities other fission products
 - SiC decomposition at high temperature
- Inter-relationships between failure mechanisms

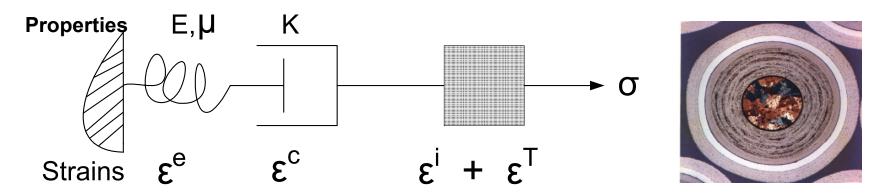






Coating Stress Modeling Requires Large Quantities of Detailed Data

Linear Viscoelastic Constitutive Equation for Coatings



Coating properties depend strongly on:

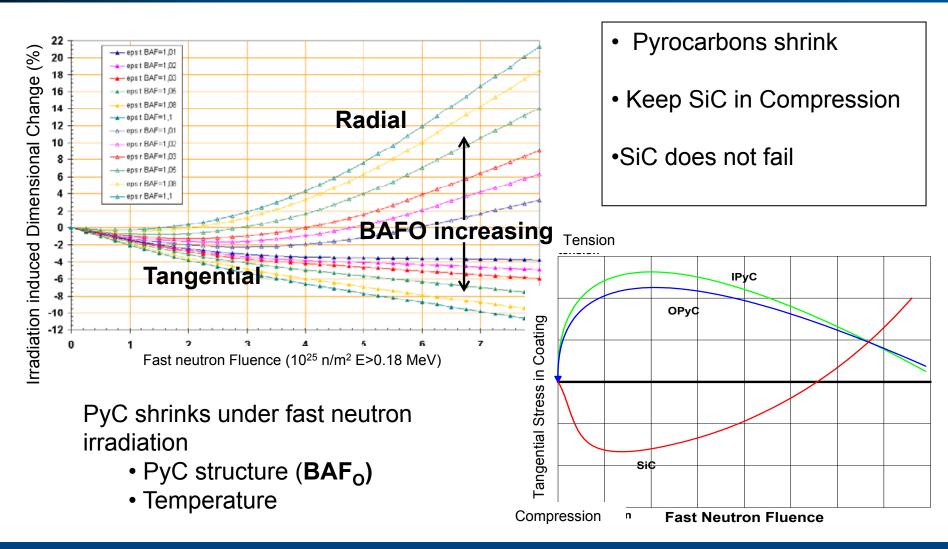
- Fabrication process that affects coating structure
- Exposure to fast neutrons
- Temperature
- Imposed stress

Failure by Brittle Material Statistical Model - Weibull

$$P_f = 1 - exp(\int_V \left(\frac{\sigma}{\sigma_o}\right)^m dV)$$

.....the coating properties constitute the largest uncertainty in predictions of coated particle performance

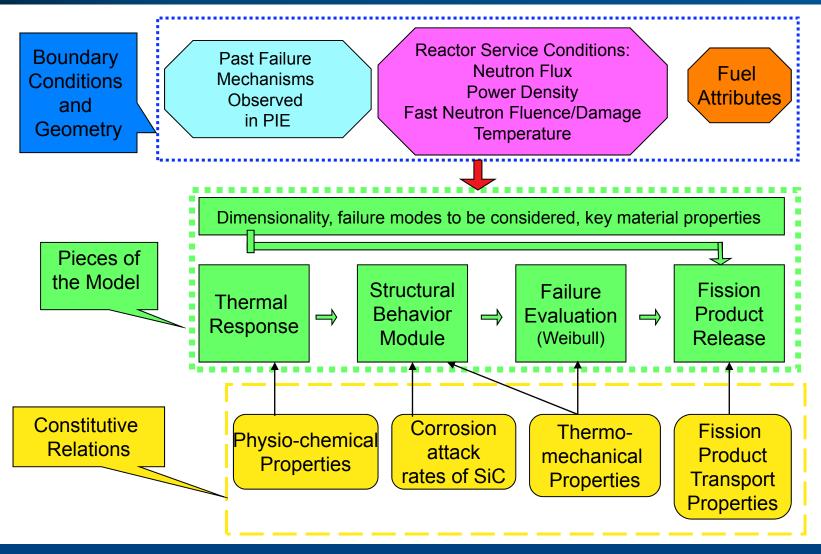
TRISO Coatings Are Complex Structures with Complex Interactions Between Coating Layers







INL PARFUME – Integrating First-Principle Treatment of Failure Mechanisms for General Applications





Accident Modeling

- Initial empirical separate effects treatments used in the past
 - Pressure vessel, chemical attack, amoeba
 - Thermal decomposition depending on accident temperature and state of irradiation
- 1-D performance codes being upgraded and integrated for applications during accidents
- Covered in Module 15





Summary – Fuel Performance Modeling

- 1-D fuel particle performance codes are being developed in many countries
 - Codes have different levels of capability
 - Goal to integrate failure mechanisms
 - Most still under development moving toward a common goal of universal applicability
- Uncertainties in performance predictions arise mainly from properties of irradiated coatings
- Multi-dimensional codes are used to predict nonspherical effects





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Fuel cycle issues



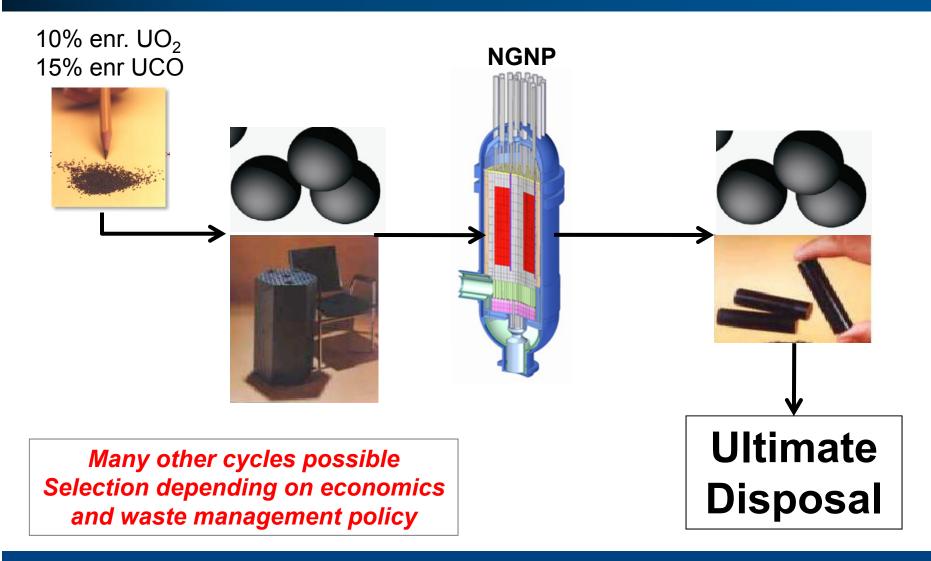


Fuel Cycle Issues

Sustainability

- Resource utilization
- Enrichment
- Thorium
- Proliferation
 - Reprocessing of coated particles
- Fuel cycle economics
- Ultimate disposal of coated particle fuel

Once-Through LEU Fuel Cycle being Considered for NGNP - Good Proliferation Resistance





Fuel Cycle Parameters

Parameter	Units	PBMR-CG (LEU)	GT-MHR (LEU)	PWR
HM loading	MT/GW(th)	11.2	7.5	36
Ore utilization	U3O8/GW(e)-Yr	183	182	212
Conversion Ratio	new fissile/used fissile	0.46	0.4	0.5
Discharged Pu	kg/GW(e)-Yr	147	96	338
Heat load - discharge@ 10 years	kw(th)/GW(e)-Yr	25	24	26



Summary

- Coated particle fuel has been manufactured in commercial quantities and successfully used in power reactors
- Substantial experience with fuel irradiation, examination, and testing → strong database on fuel performance
- Performance modeling is continuously improving – additional data and validation needed

Suggested Reading

Fuel Operating Experience in HTGRs

- A. Baxter, et al., "FSV Experience in Support of the GT-MHR Reactor Physical, Fuel Performance, and Graphite," IAEA Technical Committee Meeting on 'Proceedings of the Development Status of Modular High Temperature Reactors and Their Future Role," November 1994, ECN, Petten, Netherlands
- Nuclear Technology, 35, No. 2 206-573 (1977) entire volume

Fuel Irradiation and PIE

- D. Petti, et al., "Technical program plan for the advanced gas reactor fuel development and qualification program," Idaho National Laboratory Report INL/EXT-05-00465, Rev. 2, July 2008
- "Fuel performance and fission product behaviour in gas cooled reactors," IAEA-TECDOC-978 (1997)



Suggested Reading

Fuel Performance Modeling

- B. Boer, et al., "Stress analysis of coated particle fuel in graphite of high-temperature reactors," Nucl. Tech., 162, 276-292 (2008)
- G. Miller, et al., "Current capabilities of the fuel performance modeling code PARFUME," 2nd International Topical Meeting on High Temperature Reactor Technology, Beijing, China, September 2004
- G. Miller, et al., "Statistical approach and benchmarking for modeling of multi-dimensional behavior in TRISO-coated fuel particles," J. Nucl. Mater., 317, 69-82 (2002)
- H. Nabielek, et al., "The performance of high-temperature reactor fuel particles at extreme temperatures, Nucl. Technol., 84, 62 (1989)

Fuel Cycle Issues

- C. Ellis, et al. "Modular helium reactor fuel cycle concepts and sustainability, Proceedings of the Conference on High Temperature Reactors, Beijing, China, September, 22-24, 2004
- N. Zondi, "The Pebble Bed Modular Reactor and its alignment to the South African National Strategy for Sustainable Development, Paper G00000226, Proceedings of the Conference on High Temperature Reactors, Beijing, China, September, 22-24, 2004



