July 14, 2022 – Session 3

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ASME Code Development Status

Sec. III-5 Class SN – Nonmetallic Core Components



ASME Sec. III-5 Nonmetallic Design Rules Status

Nonmetallic Core Component Code Relevancy

- ASME Sec. III Nuclear Codes Div. 5 HTR
- Design and Materials code for the use of graphite and CMC components in HTR
- The code is process based to allow for future applications and the unique nature of the material.
- The rules are probabilistic as failure is derived from the variability in the material strength.
- It includes the evaluation of environmental effects such as irradiation, oxidation / chemical attack and stress-time-temperature (in the case of CMCs).

Technical Approach and Progress

Subsection HAB

- Revising Data Report Forms required for Certification
- Subsection HHA (Graphite)
 - Several Task Group activities ongoing to address identified optimization areas.
- New code changes and clarification
- Subsection HHB (Composites)
 - Initiated Task Group to preliminary review code for optimization areas with the development of new HTR technologies.
 - Continuation of code changes/amendments (corrections & non-mandatory appendices)



NRC Endorsement of ASME Section III, Division 5 - Status

 Since last review NRC completed its review of ASME Section III, Division 5 (2017 Edition) and accompanying Code Cases



U.S. NUCLEAR REGULATORY COMMISSION

DRAFT REGULATORY GUIDE DG-1380

Proposed Revision 2 to Regulatory Guide 1.87

Issue Date: August 2021 Technical Lead: Jeffrey Poehler

ACCEPTABILITY OF ASME CODE, SECTION III, DIVISION 5, "HIGH TEMPERATURE REACTORS" *"It endorses, with exceptions and limitations, the American Society of Mechanical Engineers (ASME) Boiler and Pressure Vessel (BPV) Code (ASME Code) Section III, "Rules for Construction of Nuclear Facility Components," Division 5, "High Temperature Reactors"" - DG-1380*

- Draft Regulatory Guide (DG-1380) and draft NUREG were issued for public comment (August 2021)
- Final reports expected fall 2022.

NRC Endorsement: Exceptions and Limitations

The NRC is <u>not</u> endorsing:

- HHA-3141, Oxidation: The provisions of HHA-3141(c) that set the weight loss limit as 30% for geometry reduction in the oxidation analysis.
- HHA-3142.4, Graphite Cohesive Life Limit: The provisions of HHA-3142.4 that set the graphite cohesive life limit fluence to the fluence at which the material experiences a +10% linear dimensional change in the with-grain direction.
- HHA-3143, Abrasion and Erosion: The provisions of HHA-3143 that set the mean gas flow velocity limit of 100 meters per second (330 feet per second) for evaluating the effects of erosion on the GCC design.
- HHA-4233.5, Repair of Defects and Flaws: The provisions of HHA-4233.5 that set a maximum allowed repair depth of 2 millimeters (0.079 inch).

Sec. III-5 HAB (General Requirements) Development and Status

- The Society needs to prepare for the first graphite certificate holder applicants.
 - Optimize data report forms to graphite and composite applications.
 - Certify and train Authorize Inspector Agencies on nuclear graphite and composite supply chain activities.
 - Roll-out requirements to the supporting Material Organizations.
- Incorporate recent NRC guidance from DG-1380.
- Extend the graphite code to include an in-service inspection surveillance program.
 - Currently nonexistent although mentioned several places in HAB.
 - Need to explicitly call out Sec. XI Div. 1 and Div. 2, although not directly applicable.

Sec. III-5 HAB Data Report Forms

- Who certifies what ??
- Role of the
 - G Certificate Holder
 - GC Certificate Holder
 - Material Organization (QMO vs CMO)
 - Authorized Inspector (I)
 - Owner (O)

Table HAB-3255-1 Document Distribution for Design and Construction of Core Components and Assemblies							
Document	Prepared by	Reviewed by	Certified by	Approved by	Provided to [Note (1)]	Available on Request	
Design Specification (HAB-3250)	0	0	0		G, GC, I, J		
Construction Specification (HAB-3340)	G	0	G	0	0, GC, MO	I, J	
Design Drawings (HAB-3340)	G	0	G	0	0, GC, MO	I, J	
Design Report (HAB-3352)	G	0	G	0	O, GC	I, J	
Material Data Sheets (HAB-3353)	G	0	G		0	J	
Construction procedures (HAB-3451)	GC, MO	G		G	G, O	I, J	
Certified Material Test Reports	MO, GC	G	MO, GC		GC, O	I, J	
Shop and field drawings (HAB-3452)	GC, MO	G		G	GC	I	
Construction Report (HAB-3454)	GC	G,0	G	0	G, O. I	I, J	
Data Report Form G-1 (HAB-8410)	GC, G	I	GC, I		0, I	J	
Data Report Forms G-2 and G-4 (HAB-8410)	GC, MO	<u> </u>	GC, MO, I		GC, I	J	
Data Report Form N-3 (HAB-8420)	0	Ι	0, I	J			

Design Specification t Design Report Numbe Construction Specific Construction Report N	CERTIFICATE HOLDER'S I	CATION OF DESIGN (18) (19) (20) (21) Designer) REPORT OF	Revision Revision Revision Revision CERTIFICATION			Se Ma F	ec III-/ ndato \pp. V	А ргу	
I, the undersigned, reg and evaluated the Co this Data Report. Foll and belief the GC Cer Section III, Division S, requirement of the De Certificate of Authoriz Date Na GC CI We certify that the sta details of materials, c. conform to the rules for herein. Certificate of Authoriz	presenting the Designer and em struction Report for the Graphiloving evaluation, the Construct tifticate Holder has constructed that the construction specification sign Specification. (22) mme	Joiyed by or Composite Core Co on Report has been cert is component in accord, on listed herein, and thes Expires Signature IFICATION OF CONSTIF dring listed C-2 and C-4 this Graphite or Compose, e, Section III, Division S, Expires	mponent or Core Ass field and to the best a ance with the rules or subscription specific econstruction specific RUCTION COMPLAI Data Reports are co and the Construction	_ have examined sembly described in of my knowldege fications meet the 	Co wit	omposite h the gra Class S Core C	es rules aphite ru N Nonn Compor	integra iles uno netallic ients.	te ler
Date Na	ime(23)	Signature		I		Form G-4	i -		Page 2 of _(
I, the undersigned, ho and employed by have inspected the Gr that to the best of my Section III, Division 5. By signing this certific	CERTIFIC Iding a valid commission issued raphite or Composite Core Com knowledge and belief this comp ate neither the Inspector nor his	ATE OF INSPECTION by the National Board of _(24)	Boiler and Pressure described in this Dited in accordance w	Date	Name	INSTAL (19)	LED BY		
the graphite or compo employer shall be liab connected with this in Certificate of Accredit	site core assembly described in le in any manner for any person spection(25) ation No(25)	this Data Report. Furthe al injury or property dama Exp (26)	ermore, neither the li age or a loss of any pires Commiss	We certify that the Core Compone Construction S	CEF statements made in ent(s) forming the C pecification and as	RTIFICATE OF INSTA this report are correct aphite or Composite sociated drawings.	ALLATION COMPLIA ct and that the installa Core Assempty lister	NCE tion of the Graphite d in this report confo	or Compostie rm(s) to the
Date Name	MACHINI 	IG PERFORMED BY	ure	GC Certificate Hol Certificate of Autho Date	ider rization No (Name	(2) GC Certificate Holder (21)	NEW R	22-1015	(G-4)
We certify that the staten rules for machining of the GC Certificate Holder Certificate of Authorizatio Date Name	CERTIFICATE OF nends made in this report are of ASME Code, Section III, Div on No(19)(GC Certificate Holder) c(19)	MACHINING COMPL correct and that all com ision 5. ExpiresSignat	AINCE iponents listed in ti	I, the undersigned, and employed by Certificate of Accre inspected the graph knowledge and bei By signing this cert the graphite or com employer shall be i connected with this	holding a valid con ditation No life or composite c ief this component ficate neither the li posite core assem able in any manne inspection.	CERTIFICATE (amission issued by th (22) (23) ore assembly describ- has been constructed spector nor his empl by described in this D r for any personal inju	DF INSPECTION e National Board of B Expires ed in this Data Report in accordance with th oyer makes any warr pata Report. Furtherr ry or property damag	oiler and Pressure V a and state that to the ne ASME Code, Sec anty, expressed or in nore, neither the Ins e or a loss of any kin	'essel Inspector , hav ∋ best of my tion III, Division nplied, concerni pector nor his d arising from c
I, the undersigned, holdin and employed by Certificate of Accreditatio	CERTIFIC/ ng a valid commission issued (2 (2) n No(21)	ATE OF INSPECTION by the National Board 0)E>	of Boiler and Press	Date,	Signed	(24 (Al)) A)	Commission(25)
nave reviewed and accept the best of my knowledge III, Division 5. By signing this certificate the graphite or comp employer shall be lia connected with this i Date	a une graphile of composite c and belief this component h neither the Inspector nor his. R21	as been machined in a employer makes and w 1-2225 Sepai	5 WG	ASME Code, Sector	oved s for	; sepa SC re	aratec eview	l into	

NEW R22-1013 (G-1)

Form G-1

Sec. III-5 HHA (Graphite) Development and Status

- Task Groups
 - Degradation: Planning & Monitoring
 - POF (Weibull & modelling)
 - Oxidation
 - Irradiated Graphite
 - Molten-salt
- Code Changes
 - Material Data Sheets
 - Clarifications

ASME Sec. III on Design & Construction and Sec. XI on In-Service Inspection (ISI) and Reliability & Integrity Management (RIM)

- ASME Strategic Objective to improve the interface between Sec. III & Sec. XI
 - Part of the 2025 Code Cycle Priorities
- Ongoing for metallics, concerns raised for transition from construction to examination are
 not well aligned
 - Sec. XI Div. 1 evolved exclusively around LWR technology.
 - Sec. XI Div. 2 (RIM), a risk-informed ISI program → initiated to couple with Sec. III for products (advanced reactor designs) not included under Sec. XI Div 1.
- Determining Safety Classification and Categorization using processes consistent with regulation is the responsibility of the Owner
 - This is ASME / US approach but may be different for others (e.g. UK etc.)

Nonmetallic (SN) Criteria Material Degradation, ISI & RIM

For Metals:

- HAA-1130 LIMITS OF THESE RULES :

"The rules of this Subpart and Subsection HH provide requirements for new construction and include consideration of mechanical and thermal stresses due to cyclic operation. They do not cover deterioration that may occur in service as a results of environmental effects such as radiation, corrosion, erosion or instability of materials."

• For Graphite and Composite Materials:

- HAB-1130 LIMITS OF THESE RULES :

"The rules of this Subpart and Subsection HH provide requirements for new construction and include consideration of mechanical and thermal stresses due to cyclic operation. They include consideration of deterioration that may occur in service as a result of environmental considerations."

	Sec III	Sec XI
For Graphite and Composite Materials ASME require As-Fabricated material properties (unirradiated) <i>Over operating temperature range</i> Irradiated material properties Oxidation effects on material properties	Design for nominal plant life using predictive models : As-fabricated Irradiated Oxidation or chemical attack Stress-time-temperature	 Plan for component surveillance using assessment models: Inspection (forewarning of severe cracking) Monitoring (deterioration of the graphite and impact on the overall condition) Structural Assessment (damage predictions) Consequences (Consideration of observed and postulated deterioration of
	4	ADVANCED REACTOR TECHNOLOGIES

WG-NDM Task Group on Material Degradation & Failure Monitoring TPOC: Martin Metcalfe

- Only the designer can define what/how a component fails
 - Single crack / multiple cracks / crack in a specific orientation
- Meaning of "failure", "functionality" and "damage tolerance" needs to be unambiguous:
 - Probability of Failure = Probability of Crack Initiation (R22-486 in progress)
 - Damage tolerance levels depend on core design and functionality
 - A crack in the graphite components does not necessarily result in the loss of component function. *Ultimately the loss of function is component failure.*
- Monitoring and surveillance programmes should be an integral part of the core design
- Multi-legged safety cases (inspection, monitoring, assessment, consequences)
- Designers will have to design to some nominal lifetime, but also with some consideration of lifetime margins. Plant operators will certainly wish to plan for economically beneficial life extensions.
- Initial focus on graphite (composites to follow)
- Martin Metcalfe, "Damage Tolerance in the Graphite Cores of UK Power Reactors and Implications for New Build" whitepaper in review, publishing NED TBD.

Cracked AGR core brick at Hunterston B power station

Reliability and Integrity Management (RIM)

- Many of these new rules are not applicable for construction rules (Section III)
- Discussing new rules within Section XI, Division 2 (RIM)
 - Long term degradation rules
 - RIM data required to determine failure
 - RIM data to determine if failure has occurred
- End-of-life irradiation and oxidation degradation rules



TPOC: Andrea Mack

Aug 2022, virtual meeting

Graphite workshop (Weibull & POF)

WG-NDM Task Group on POF (graphite)

Allowable stress calculation: 3-parameter method



range

parameter,

 $\Delta = 0.2$

Errata

- The code provides a method to always use a conservative stress distribution, but the current process is not a quantifiable conservatism.
- POF without volume grouping is less conservative
 - finer mesh = higher POF (more conservative)
 - Stress range parameter determines volume group size (mesh size), not V_m



WG-NDM Task Group on the Modification of Oxidation

Regime 3

(Rate)

5

Oxidation is local

- Irradiation is not local
- Weight loss is local
 - Intrinsic factors (microstructure, raw materials, forming method)
 - Extrinsic factors (temperature, oxidant supply, flow conditions, shape and size)



R21-1392 SC approved – On path for 2023 ed.

Regime 2

Regime

1/T-



Numerous results in the literature conclude that the strength of various grades of uniformly oxidized graphite specimens drops to 50 % of initial strength at 10 % weight loss.



FORM MDS-1 MATERIAL DATA SHEET (SI UNITS)

- Property Degradation versus Weight Loss % in Uniformly Oxidized Graphite

- C. Contescu, R.Paul, "Oxidation Behavior and Property Degradation of Nuclear Graphites", ORNL/TM-2022/1839
- Ryan M. Paul et al., "On the Thermal Oxidation of Nuclear Graphite Relevant to High-Temperature Gas Cooled Reactors" whitepaper in progress, publishing TBD.

WG-NDM Task Group on Irradiated Graphite

Objective: To revise the code to require an applicant to provide limited irradiation data to ascertain similar behavior (significant cost and time reduction for material qualification).

Aim to establish turnaround with only a few data points to (1) confirm data trend and (2) reduce the burden of large irradiation experiments.

Implementing Dimensional Change Theory

$$\frac{dG_x}{d\gamma} = A_x \left(\frac{1}{X_c} \frac{dX_c}{d\gamma} \right) + (1 - A_x) \left(\frac{1}{X_a} \frac{dX_a}{d\gamma} \right) + f_x$$

W. Windes, A. Campbell, S. Johns

- Establish lower bound design constraints (95% lower limit)
- Determine turnaround → tricky due to irradiation experiment temperature control

Effort ongoing: to be repeated with strength, elasticity, CTE and thermal diffusivity

Several whitepapers & code changes expected for 2025 ed.

R19-2810 in progress (Review of irradiation dependent strength increase)



TPOC: Nidia Gallego

WG-NDM Task Group on Molten Salt

Graphite materials workshop Upcoming July 2022, virtual meeting

- Salt impregnation into graphite pores
 - Physical damage/cracks
 - "Hot spots" from fueled molten salt
- Wear/abrasion/erosion
 - Molten salt has higher density than graphite
 - Liquid flow over soft graphite has potential
- Chemical coupling with metallic systems
 - Graphite MS is inert but ...
 - There are questions when a metallic component is added

The current HHA does not address any coolant salt interactions with graphite.

Chemical attack, salt infiltration and retention as well as wear and erosion aspects need to be incorporated in the design rules.





Salt residue



Before immersion in FLiNaK

After immersion in FLiNaK

2023 Code Changes & Clarifications



2023 Code Changes – ASME Materials Data Sheets (HHA-II)

- Elevated temperature testing
 - Graphite gets stronger with increasing temperature
 - Very difficult to test:
 - No test standards
 - Very little advantage
 - Modulus increases
- This is optional
 - Since strength increases with temperature, if elevated temperature strength **is not used** then considered conservative.

		FORM MDS	-1 MATERIA	L DATA SH	EET (SI UN	ITS)		
			Grade	Designation				
Material Grade		Material spec	. ID F	F AS	STM spec		н	
Max. grain size (mm)	퀵		Des	Designation		F		
		Те	mperature-De	pendent Par	ameters			
Property	Units	Orientation	20°C	200°C	400°C	600°C	800°C	1000°C [Note (1)]
Bulk density 🕞	kg∙m ⁻³		<u> </u>					
Strength – tensile F	MPa	WG, AG						
Strength – flexural ा (4-point)	MPa	WG, AG						
Strength – compressive 🖻	MPa	WG, AG						
Elastic modulus 🕞 (dynamic)	GPa	WG, AG						
Elastic modulus (static) F	GPa	WG, AG						
Coefficient of thermal F	°C-1	WG, AG						
Thermal conductivity 🗗	W/m•k	WG, AG						

R19-2806 under review for first iteration ballot at Sec. III

Future Code Changes

Graphite Oxidation – Effect						
Property	Units	2%	4%	6%	8%	10%
trength [.] 🍺						
lastic modulus (dynamic) [.] 🗗						
hermal conductivity [.] 🝺						
		Irradia	ted Graphite			
Property		Unite	WG		AG	

Material property after oxidation

- <u>Must be performed at lowest temperature possible.</u>
- Maximum oxygen penetration and maximum effect on material properties

Irradiation effects

- Behavior should be represented as plots dependent upon received dose and irradiation temperature
- Writing code rules to establish a universal response for all grades of graphite

Sec III-5 HHB (Composites) Development and Status

- Code Changes
 - Loading mode stress
 - Non-mandatory appendices
- Task Group
 - Composites (Technical Basis and Benchmarking)
 - Synergies
 - Future:
 - POF
 - Degradation: Planning and Monitoring

2023 Code Changes – Failure Mode Stress (Composites)

Graphite

Composites

Technical Requirements

Graphite Core Components

Graphite Core Assembly

Maximum deformation energy theory (equivalent stress) - Design by Analysis

- Simple assessment
- Full assessment
- Design by test

Composite Core ComponentsPCMC ComponentsFailure Mode Stress Theory
(equivalent stress do not apply)- Design by Analysis
- Simple assessment

Figure HHB-3221-1 Allowable Stresses Flowchart for SRC-1 and SRC-3 Composite Core Components

- Design by test



Graphite uses the maximum deformation energy theory that combines stresses. This allows for an arbitrary stress state at a point to be converted to an equivalent stress which is then directly compared to the results of a uniaxial strength test. (HHA-3213)

- HHA Simple Assessment: calculate the peak equivalent stress
- HHA Full Assessment: calculate the combined equivalent stress

Composites design approach requires comparing the maximum stresses resulting from the loading of the component to the stress at failure of the material. It <u>does not make use of the theory for</u> <u>combining stresses</u>. The stress at failure needs to be determined for the mode at failure exercised by the applied stress. (HHB— 3213)

HHB Simple assessment: calculate the maximum loading mode stress

The equivalent stress approach should not be used in HHB.

The ratio of strengths is not applicable to composites

HHB C-C CMC Non-mandatory Appendices

HHB-D C-C Materials and Applications HHB-E C-C Irradiation and Environmental Effects

CMC Irradiation and Environmental Effects

Campbell Anne A. and Burchell Timothy D. (2020). Radiation Effects in Graphite. In: Konings, Rudy JM and Stoller Roger E (eds.) Comprehensive Nuclear Materials 2nd edition, vol. 3, pp. 398–436. Oxford: Elsevier.



C-C composite following irradiation (at 500°C and 800°C)

L.L. Snead et al. / Journal of Nuclear Materials 321 (2003) 165-169

L. Snead, Ceramic structural composites: The most advanced structural material, presented at the International School on Fusion Reactor Technology, Erice, Italy, July 26–August 1, 2004.

T.D. Burchell, Radiation damage in carbon-carbon composites: Structure and property effects, Physica Scripta 64, 17–25, 1996.

T.D. Burchell., Irradiation-induced Structure and Property Changes in Tokamak Plasma-facing, Carbon-Carbon Composites, Moving Forward with 50 Years of Leadership in Advanced Materials, 39th International SAMPLE Symposium and Exhibition, vol. 39, Books 1 and 2, pp. 2423–2436, 1994.

T.D. Burchell, T. Oku, Materials Properties Data for

Fusion Reactor Plasma Facing Carbon-Carbon

Composites, International Atomic Energy Agency, pp. 77–128, 1994.



R20-1307 (HHB-D & HHB-E) SC reviewed – On path for 2023 ed.

WG-NDM: Task Group on Composites

The composites task group is <u>a subset of the nonmetallic</u> <u>design and materials working group (NDM-WG)</u> with specific focus <u>to address mission relevant activities</u> as it relates to Sec III.5 HAB and HHB on ceramic matrix composites.

Objective:

- Bring vendor community together on code related questions
- Identify type/current composite applications and code related issues that have been uncovered
- Identify areas that require review and/or further optimization
- Discuss strategies to demonstrate or benchmark the code methodology.

Monthly occurrence

Examples of Fiber Architecture



- Qualification Methodology:
 - Is it possible to optimize and/or accelerate the qualification process by reducing the material qualification effort?
 - How can technologies & analytical methods be used to reduce testing efforts?
 - What is truly mandatory or non-mandatory in the code?
- Composite design rule assessment
 - Does the "simplified assessment" design approach clearly explain how to address anisotropic differences in mechanical properties?
 - Is there sufficient detail for the design by test methodology?
 - When should which method be applied?
- Industry: code practicability and readiness
 - Identify optimization areas.

TPOC: Josina Geringer

±45 deg

WIC composite

(SiC-SiC)

40

30 ś

20

10

Stress,

WG-NDM Task Group on Composites

HHB-3214.7 Combined Stress (Cm + Cb). The combined stress is the sum of all of the components of stress at a point. In design, it is customary to distinguish between primary and secondary stresses. These are defined as follows:

(a) Primary stress is any normal stress or a shear stress developed by an imposed loading that is necessary to satisfy the laws of equilibrium of external and internal forces and moments. The basic characteristic of a primary stress is that it is not self-limiting. Primary stresses that considerably exceed the material strength will result in failure A thermal stress is not classified as a primary stress.

(b) Secondary stress is a normal stress or a shear stress developed by the constraint of adjacent material or by self-constraint of the structure. The basic characteristic of a secondary stress is that it is self-limiting. Local yield-

ing and min cause the st

Due to th distinctio stresses fo Combined stress and

Could a higher POF be applied to interlaminar stresses if they:

- Are self-relieving / self-limiting?;
- Do not induce fiber-dominated failure? and:
- Do not compromise the component's ability to function?

Internal Stresses due to Irradiation



Radial direction develops compressive stress

For composite materials, matrix failure modes are not always catastrophic.

- How is this applied elsewhere?
- What does NASA and FAA apply?



HHB-3214.2 Maximum Loading Mode Stress. The maximum loading mode stress in a Composite Core Component is the highest loading mode stress computed from

cordance wi This stres of the loads maximum lo most severe loadings or mode?

vice Level.

the total str • How is Maximum Loading Mode (MLM) stress determined and is it a singular global value? Or is there an MLM stress for each direction and loading

> no Maximum Loading σ max tensile (xx,yy,zz), Mode Stress σ max compression (xx,yy,zz), σ max shear (x-y, x-z, y-z, y-z, z-x, z-y) Design Allowable Sgm tensile (xx,yy,zz), Stress (Reliability Sgm compression (xx,yy,zz), Factor) Sgm shear (x-y, x-z, y-z, y-z, z-x, z-y)



Figure HHB-II-3300-1

Stress-Strain Curves for WIC Composites

0 dea/90 dea

300

200 MPa

100

n

Stress,

Tension

(X-direction)

Tension

(Z direction)

CMC Synergistic Activities & Industry Alignment



Code Week Meetings

Development of the design ASME BPV code for graphite and ceramic composite core components were discussed and coordinated at several ASME hosted virtually or in-person during 2021 and 2022.

Meeting Date	Organization: committees	Location
25-30 Jul 2021	ASME: WG GR GCCCCA, WG-NDM, SG-HTR, BPVIII	Virtual (Zoom), NY
1-4 Nov 2021	ASME: WG GR GCCCCA, WG-NDM, SG-HTR, BPVIII	Virtual (Zoom), NY
6-11 Feb 2022	ASME: WG GR GCCCCA, WG-NDM, SG-HTR, BPVIII	Virtual (Zoom), NY
1-5 May 2022	ASME: WG GR GCCCCA, WG-NDM, SG-HTR, BPVIII	New Orleans, LA
7-12 Aug 2022	ASME: WG GR GCCCCA, WG-NDM, SG-HTR, BPVIII	Virtual (Zoom), NY
5-12 Nov 2022	ASME: WG GR GCCCCA, WG-NDM, SG-HTR, BPVIII	Pittsburg, PA

Workshops associated with respective Task Groups planned:

- Molten Salt Workshop (July 2022)
- Weibull Graphite Experts (August 2022)

Virtual meeting in August and in person meeting in November (Pittsburg)

Foreseeable future two in-person and two virtual meetings per year.

