

# Tribological characterization of graphite in dry argon and molten salt environments

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**GAS-COOLED REACTOR**  
ADVANCED REACTOR TECHNOLOGIES PROGRAM



U.S. DEPARTMENT OF  
**ENERGY**

# Initial tribological studies of graphite in dry argon and molten salt environments

## Objectives:

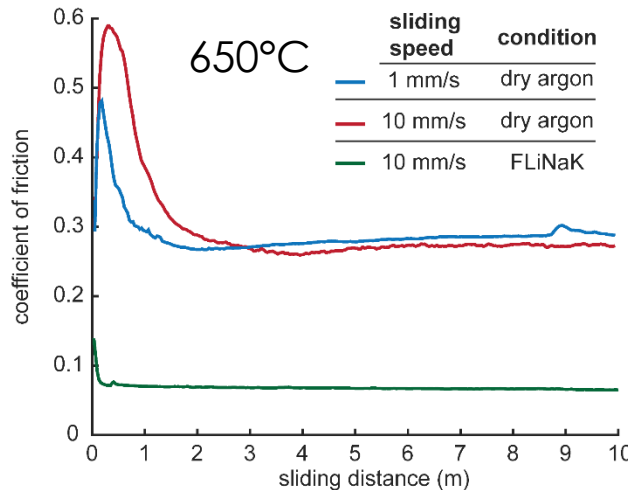
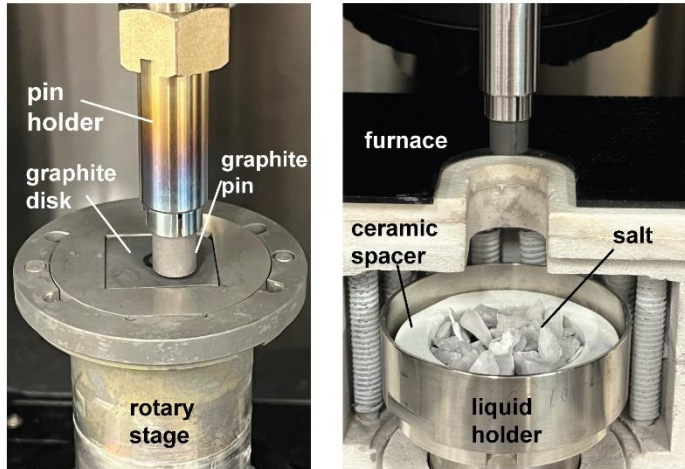
- Investigate the tribological (wear and friction) behavior of graphite pebbles in conditions similar to High Temperature Gas-cooled Reactor (HTGR) and Molten Salt Reactor (MSR) environments.

## Approach:

- Determine tribologically relevant conditions.
- Conduct wear and friction experiments on graphite in dry argon and molten FLiNaK salt environments.

## Accomplishments:

- Determined sliding/rolling speeds and contact loads of pebbles in HTGR and MSR.
- Performed initial tribological testing of graphite in dry argon and molten FLiNaK salt environments.
- Completed Milestone Report: Initial tribological studies within molten salt environment.



ORNL/TM-2024/3253

## Report on Initial Tribological Studies of Graphite in Dry Argon and Molten Salt Environment

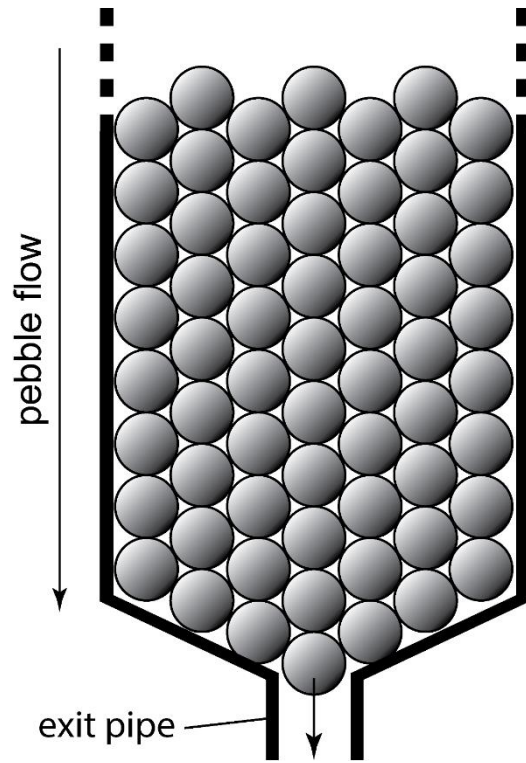


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January 2024

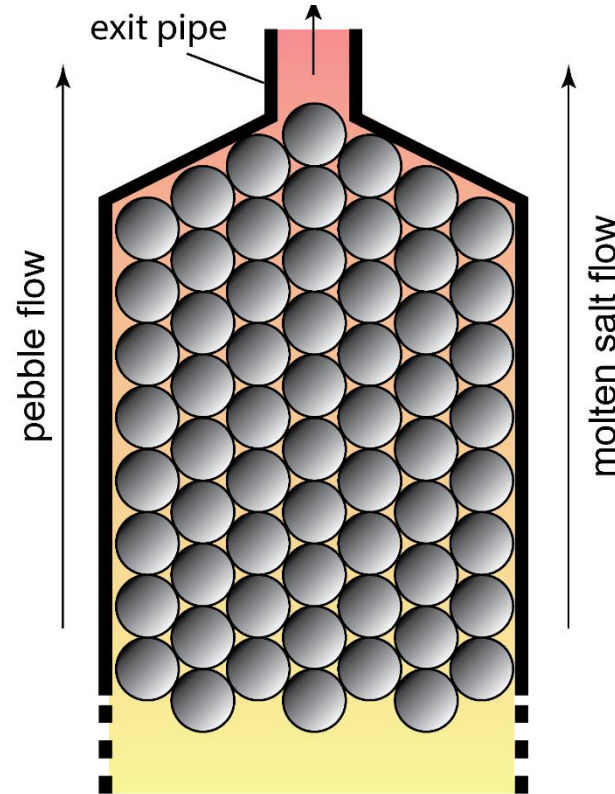
# Pebble-bed high temperature reactor

## Gas-cooled reactor



- Cooled with inert gas (He)
- Pebbles flow downwards.
- Operating temperatures 550 - 900°C.

## Molten salt reactor



- Molten salt used as the coolant.
- Pebbles flow upwards.
- Ar gas environment.
- Operating temperatures 550 - 650°C.

## Molten salts

**Fluoride salts:** FLiNaK, FLiBe

### Advantages:

- Allow lower operating pressures
- Low neutron absorption
- Allow higher burnup rates
- High thermal conductivity
- Chemical stability
- Serve as a lubricant

### Disadvantages:

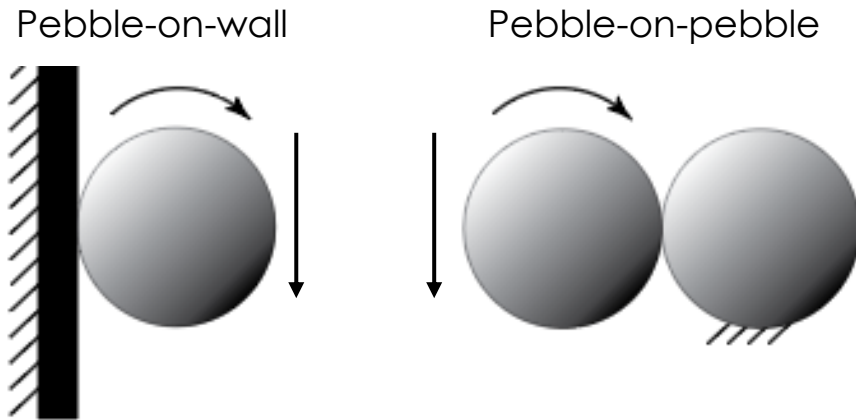
- Hazardous substance.
- Causes degradation and corrosion of graphite and other structural materials.



# Why tribological characterization?

## Graphite wear

### Sliding & Rolling



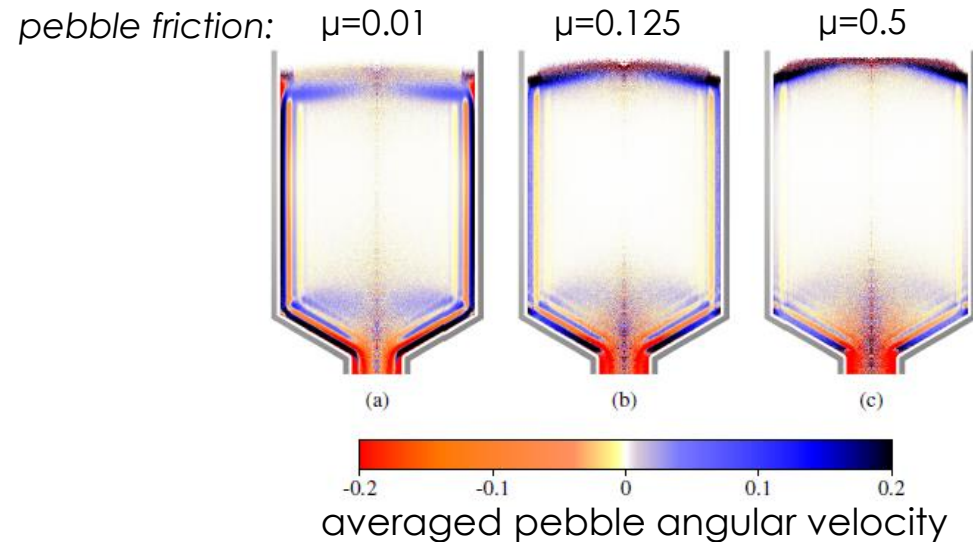
Pebbles slide and roll against other pebbles and the graphite wall during circulation in the reactor.



**abrasive wear, surface damage, generation of dust**

## Pebble flow

- Friction of pebbles and graphite wall affects the pebble movement in the reactor.
- The tribological behavior of pebbles is a critical parameter related to the motion of the pebbles, which affects their trajectory and accumulation.
- Understanding pebble flow dynamics is essential for reactor core design, pebble drainage cycle, and safety assessment.



Y. Tang, L. Zhang, Q. Guo, B. Xia, Z. Yin, J. Cao, J. Tong, C. H. Rycroft, Analysis of the pebble burnup profile in a pebble-bed nuclear reactor. *Nucl. Eng. Des.* **345**, 233–251 (2019).

# Graphite-on-graphite in dry argon environment

Contents lists available at [ScienceDirect](http://ScienceDirect)

Tribology International

journal homepage: [www.elsevier.com/locate/triboint](http://www.elsevier.com/locate/triboint)

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## Self-lubrication of nuclear graphite in argon at high temperature

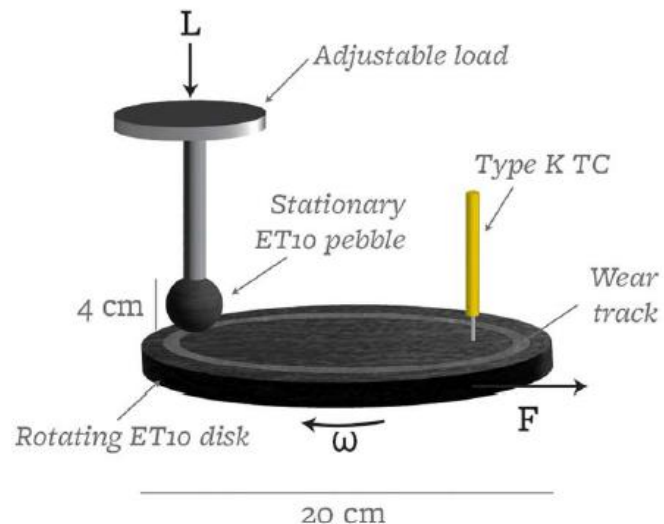
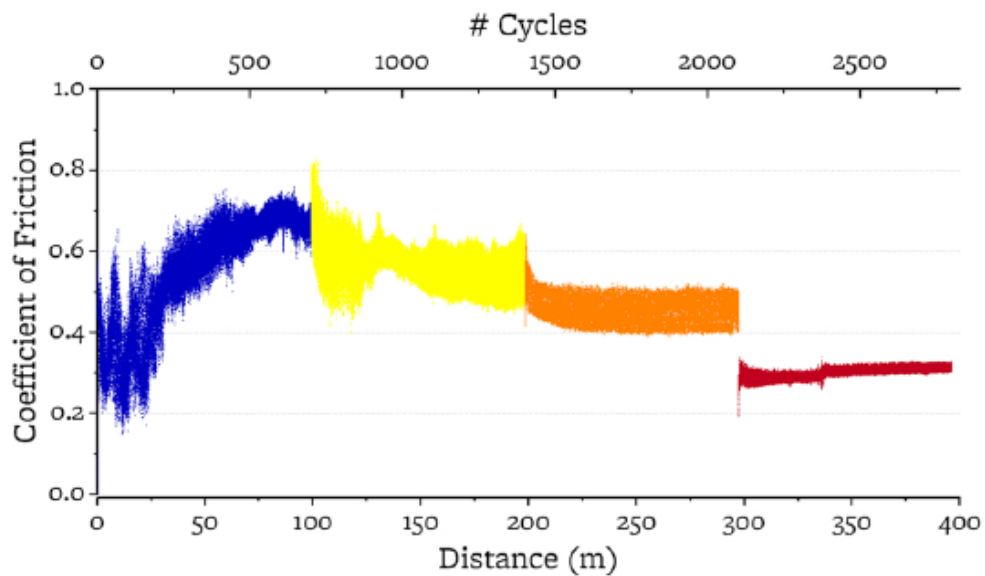
L. Vergari<sup>a</sup>, J. Quincey<sup>b</sup>, G. Meric de Bellefon<sup>b</sup>, T. Merriman<sup>c</sup>, M. Hackett<sup>b</sup>, R.O. Scarlat<sup>a,\*</sup>

<sup>a</sup> Nuclear Engineering Department, University of California Berkeley, Berkeley, CA, USA

<sup>b</sup> Kairos Power LLC, Alameda, CA, USA

<sup>c</sup> Tribology Associates, Columbus, OH, USA

T	20 °C	200 °C	400 °C	600 °C
Avg. COF:	0.55±0.13	0.57±0.05	0.46±0.03	0.30±0.01



Temperature = 20 - 600 °C

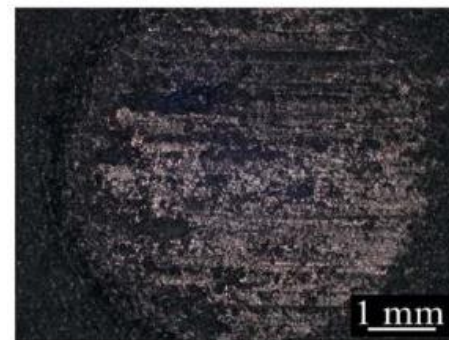
Normal force = 50N

Sliding speed = 0.15 m/s

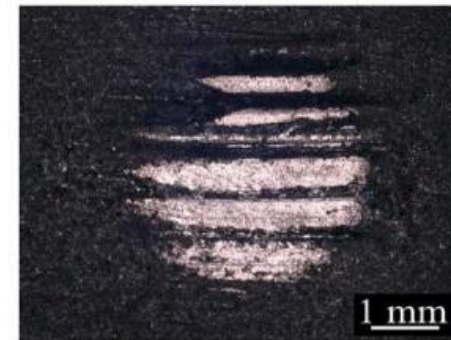
Sliding distance = 150 m

Environment: argon

**WEAR @RT**  
COF = 0.55(14)  
Wear Rate = 0.4(3) mg/Nm



**WEAR @HT**  
COF = 0.33(5)  
Wear Rate = 0.06(3) mg/Nm



# Graphite on 316H SS in molten FLiNaK salt.



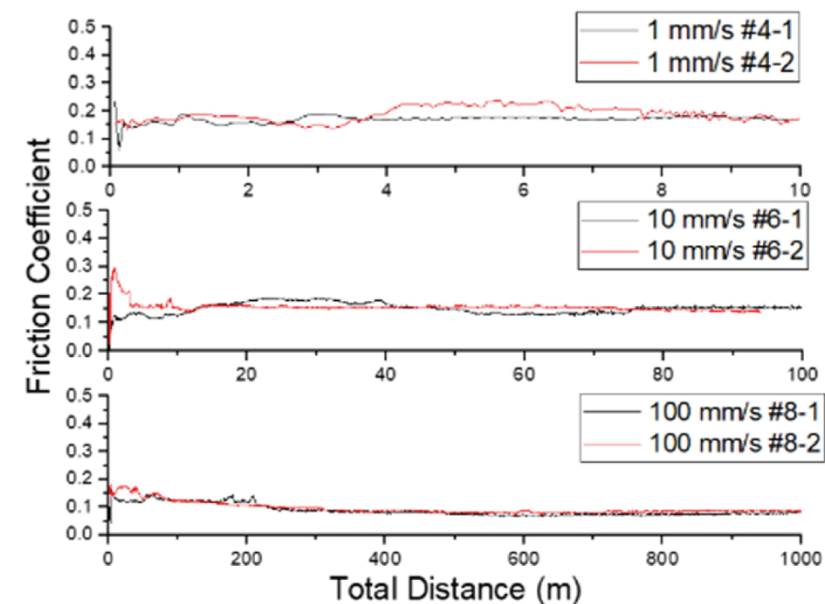
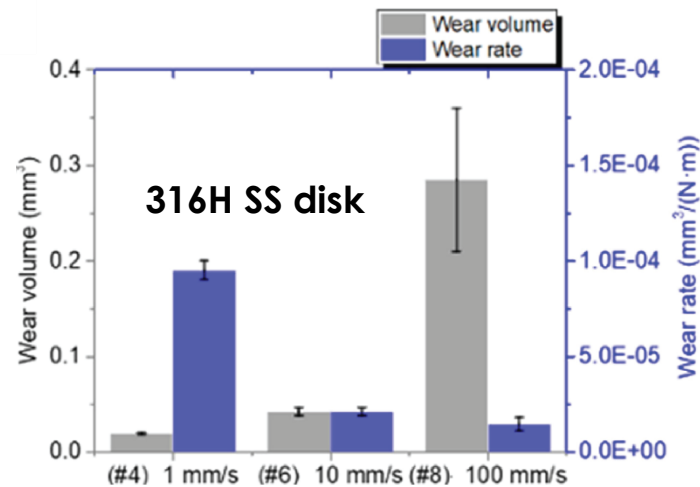
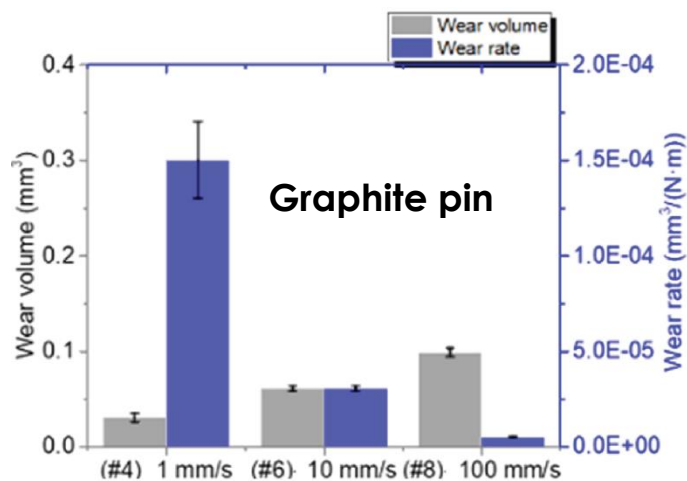
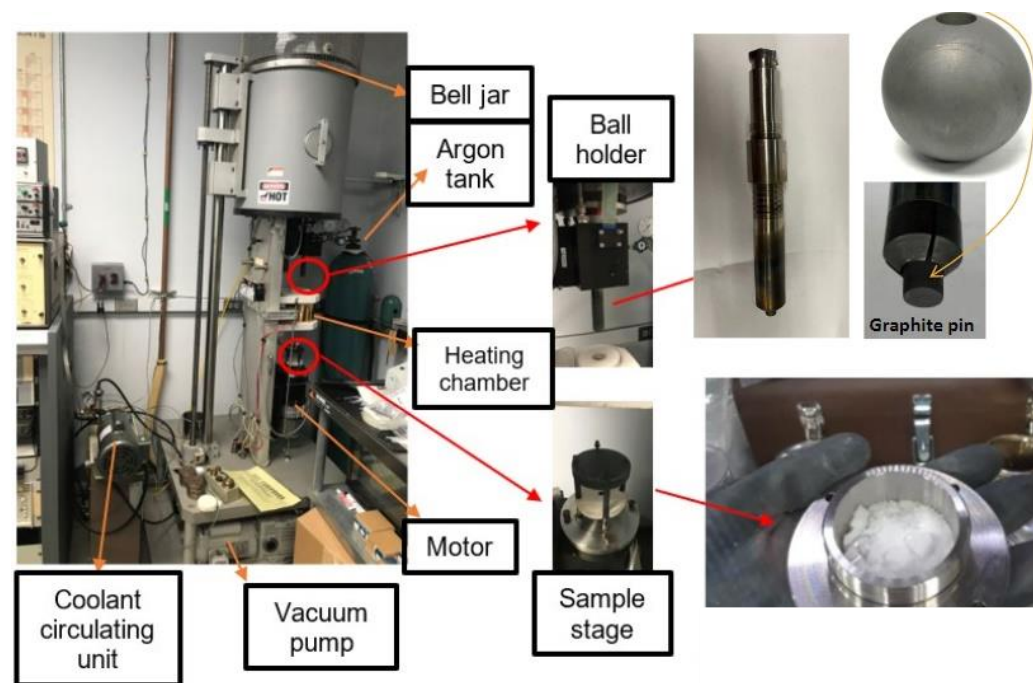
Wear  
Volume 522, 1 June 2023, 204706



## Tribocorrosion of stainless steel sliding against graphite in FLiNaK molten salt ☆

Xin He <sup>a</sup>, Chanaka Kumara <sup>a</sup>, Dino Sulejmanovic <sup>a</sup>, James R. Keiser <sup>a</sup>, Nidia Gallego <sup>b</sup>, Jun Qu <sup>a</sup>

Temperature = 550 and 600 °C  
Normal force = 20N  
Sliding speed = 1, 10 and 100 mm/s  
Environment: molten FLiNaK salt/argon

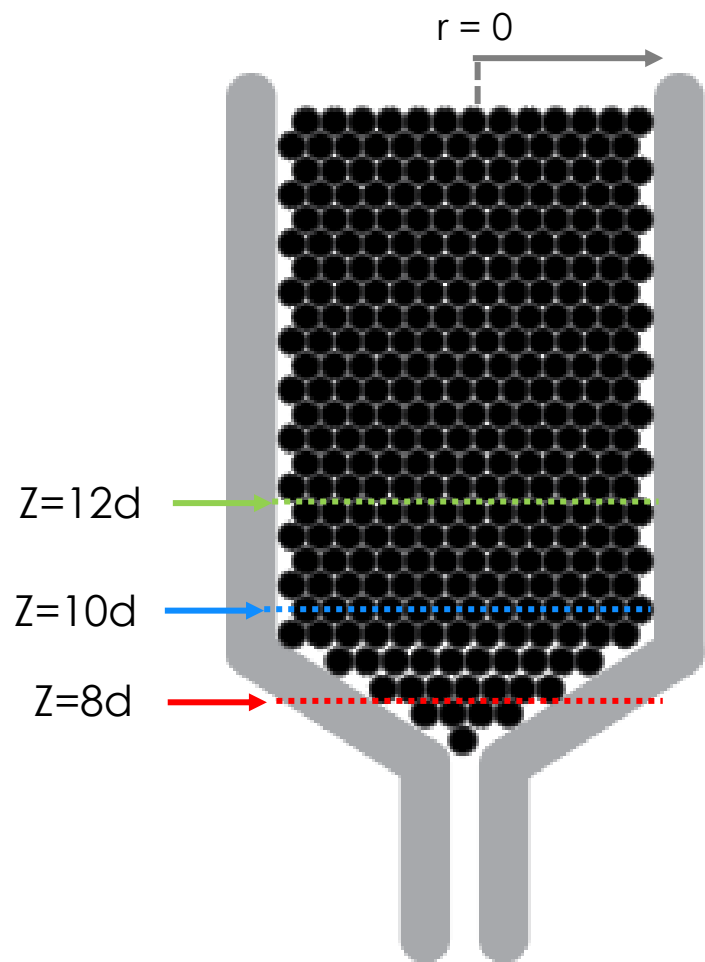


# Determination of tribologically relevant conditions

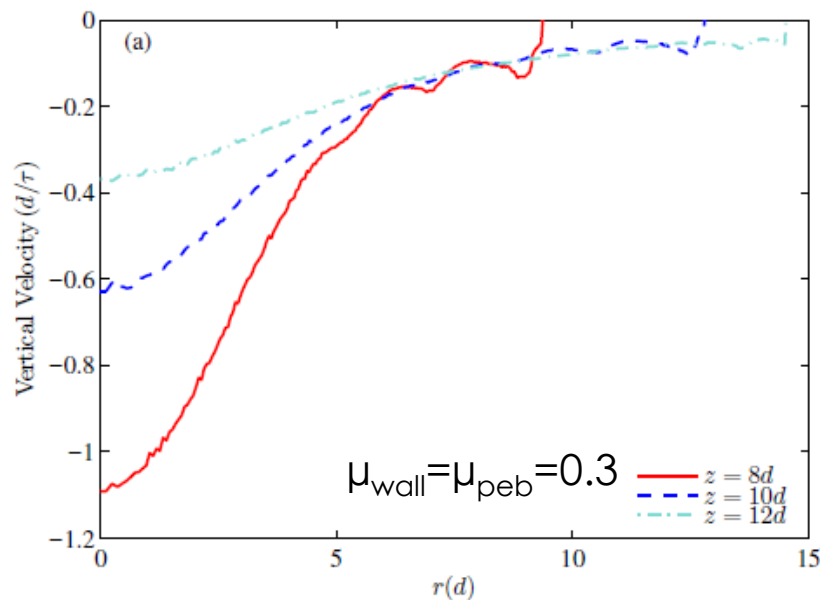
## **Unknown conditions/parameters:**

- How do pebbles move and interact with each other in HTGR and MSR?
- Is sliding or rolling the dominant contact mode?
- What are the sliding and rolling speeds?
- What is the pebble-on-pebble and pebble-on-wall pressure/load?

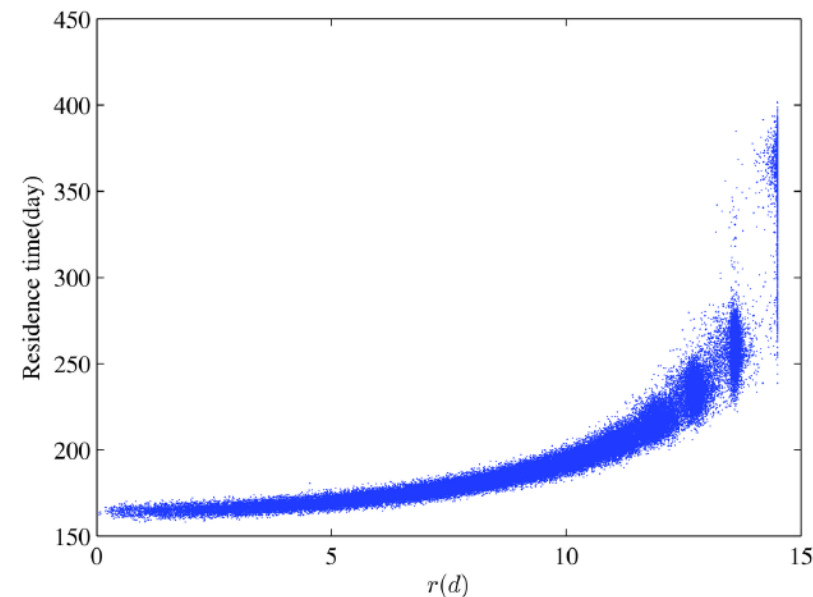
# Determination of sliding speed



Pebble vertical velocity



Pebble residence time



- Pebble sliding speeds are the highest at the center ( $r(d)=0$ ) and bottom ( $z=8d$ ) of the reactor core.
- Pebble residence time in the core is the lowest at the center of the reactor core.

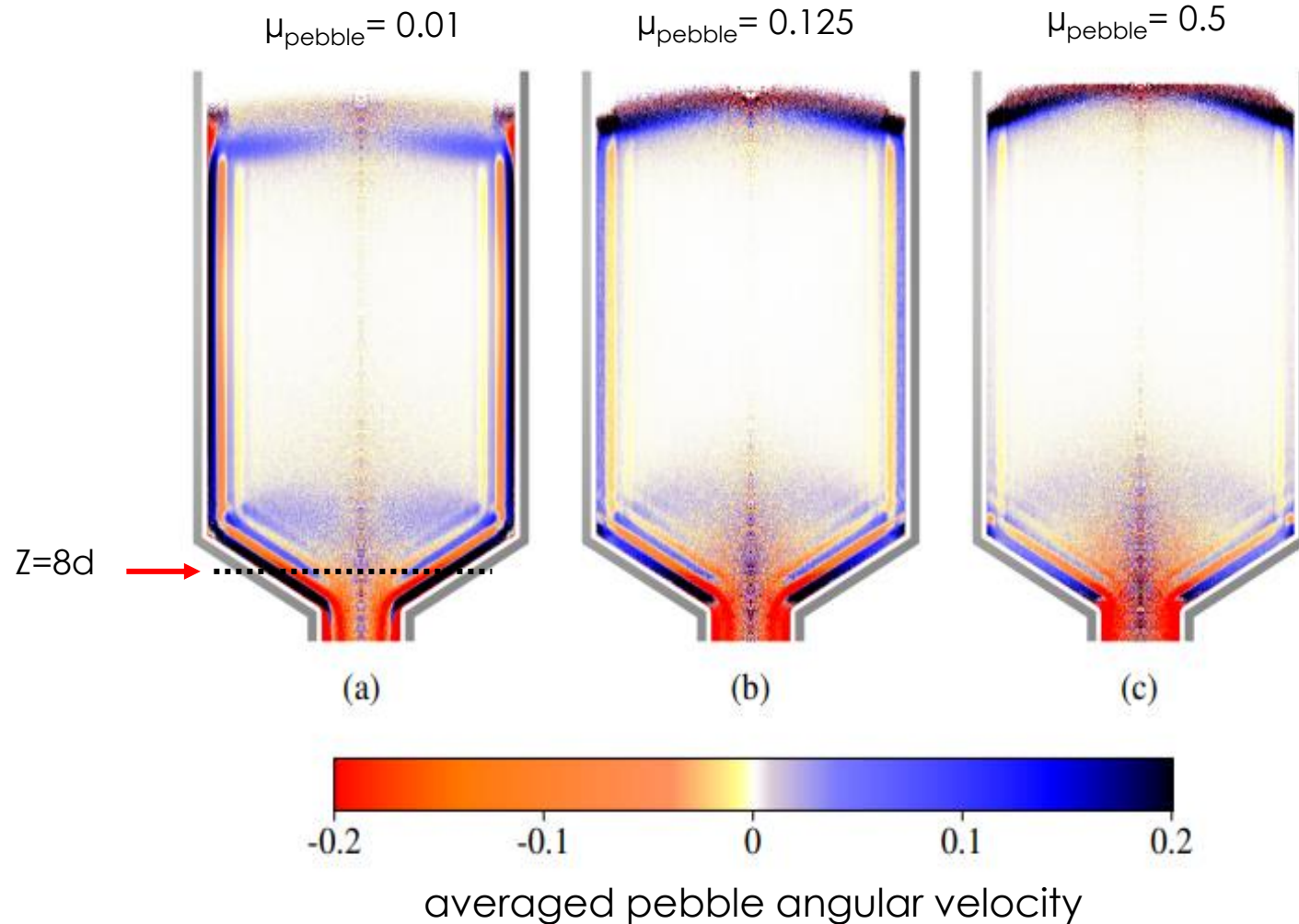
**Sliding speeds = 0.1 - 1  $\mu\text{m/s}$**

Y. Tang, L. Zhang, Q. Guo, B. Xia, Z. Yin, J. Cao, J. Tong, C. H. Rycroft, Analysis of the pebble burnup profile in a pebble-bed nuclear reactor. *Nucl. Eng. Des.* **345**, 233–251 (2019).



# Determination of rolling motion

## Angular velocity



- Pebble angular velocities are the highest at the reactor's wall (for low  $\mu$  values) and on the top and bottom of the reactor.
- Angular velocities decrease with increasing friction coefficient.

**Rolling speeds = 0.05 – 0.1  $\mu\text{m/s}$**

Y. Tang, L. Zhang, Q. Guo, B. Xia, Z. Yin, J. Cao, J. Tong, C. H. Rycroft, Analysis of the pebble burnup profile in a pebble-bed nuclear reactor. *Nucl. Eng. Des.* **345**, 233–251 (2019).

# Determination of contact force

Inputs from:

Y. Tang, et al., Analysis of the pebble burnup profile in a pebble-bed nuclear reactor. *Nucl. Eng. Des.* **345**, 233–251 (2019).

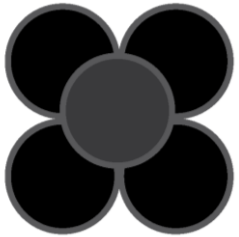
# of pebbles ( $N_c$ ) = 30,000

Pebble diameter = 60 mm

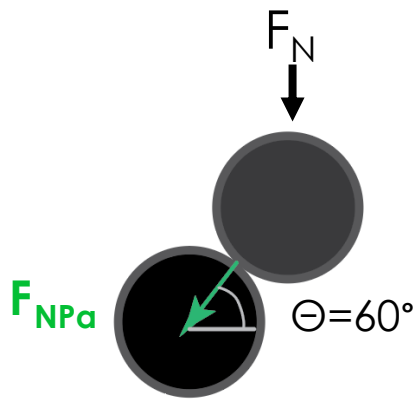
Pebble mass = 210 g

## Pebble configuration

Top view



Side view



$L_{cyl} = 2.5 \text{ m}$

$D_c = 1.8 \text{ m}$

$L_{pipe} = 0.15 \text{ m}$

$0.6 \text{ m}$

$30^\circ$

cross-sec. area of a pebble

$$A_v = 0.0028 \text{ m}^2$$

cross-sec. area of the core

$$A_c = 2.5 \text{ m}^2$$

# of pebbles in the cross-section

$$N_{cross-sec} = \frac{A_c}{A_v} \sim 900$$

total load of the pebbles in the reactor

$$F_{NC} = N_c * mass_{peb} * 9.81 \sim 50 \text{ kN}$$

load on a pebble in the bottom of reactor

$$F_{NP} = \frac{F_{NC}}{N_{cross-sec}} \sim \mathbf{55 \text{ N}}$$

$$\mathbf{F_{NP\alpha} = 1/4(F_{NP})/\cos(\theta) \sim 28 \text{ N}}$$

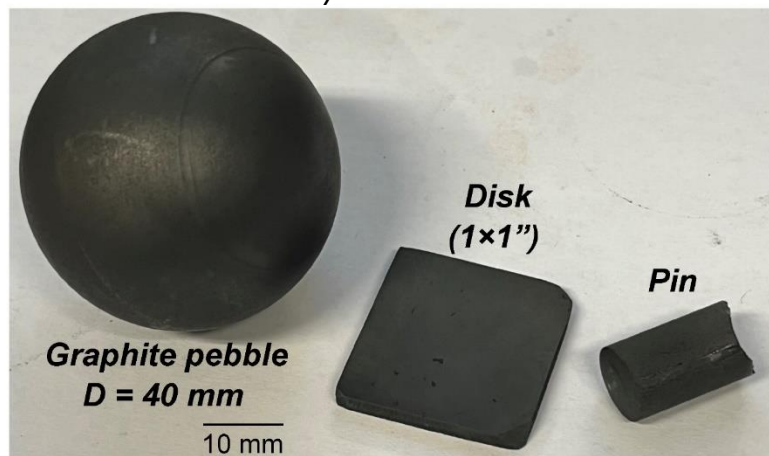
# Estimated conditions

	<b>Gas-cooled reactor (modeling data from Tang et al.)</b>	<b>Molten salt reactor (discussion with Kairos Power)</b>
<b>Contact load (N)</b>	~28	<100
<b>Sliding speed (mm/s)</b>	$<1.2 \times 10^{-3}$	$\sim 4.0 \times 10^{-4}$
<b>Rolling speed (mm/s)</b>	$<1.1 \times 10^{-4}$	N/A
<b>Travel distance (m)</b>	~10	~18
<b>Temperature (°C)</b>	550-900	550-650

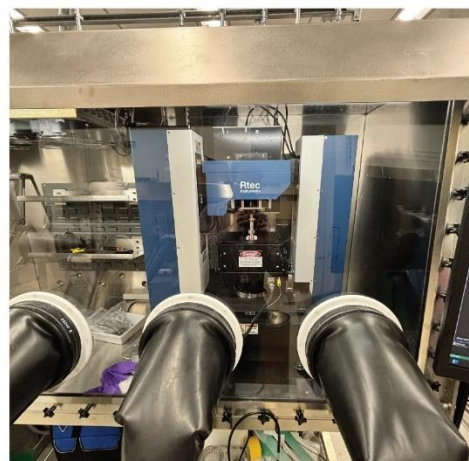
# Experimental setup

## Samples (nuclear graphite ET-10)

Provided by Kairos Power



## Tribometer in a glovebox



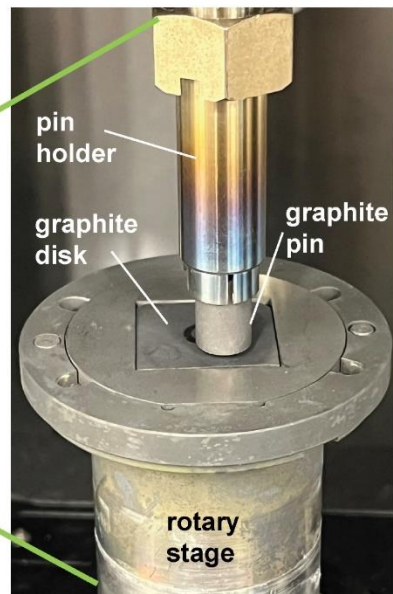
## Test conditions

Gas: argon                      Sliding speed: 1 & 10 mm/s  
Temperature: 650°C          Sliding distance: 10 m  
Normal load: 20 N

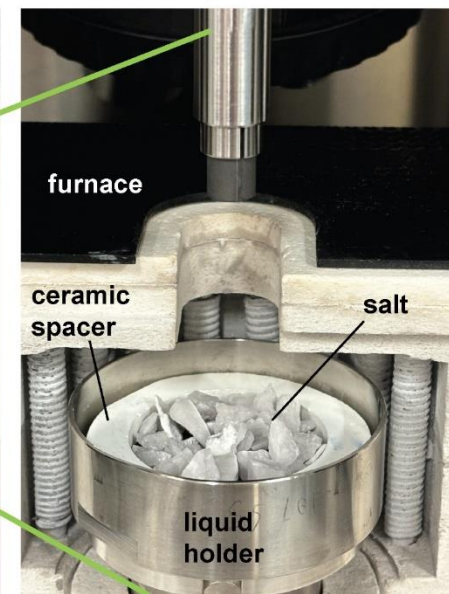
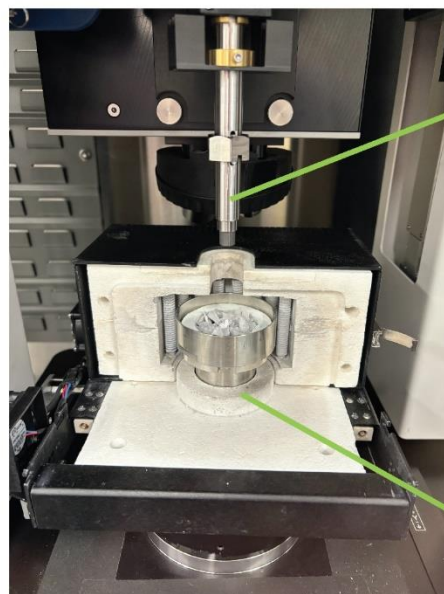
## Molten salt

FLiNaK (mol %: 46.5% LiF, 11.5% NaF, 42% KF)  
Melting point: 454 °C  
Viscosity: 3.66 mPa·s @ 650 °C

## Dry argon environment



## Molten (FLiNaK) salt argon environment



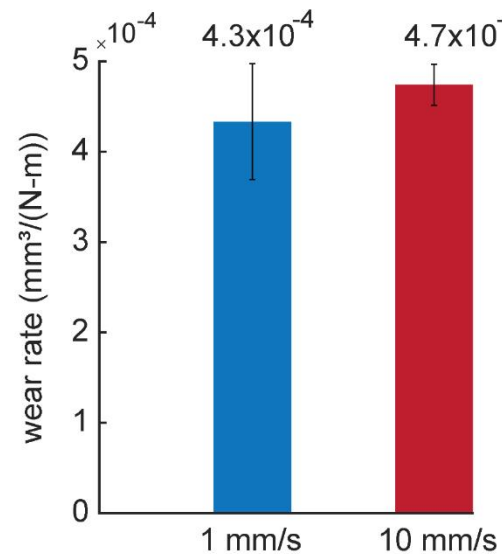
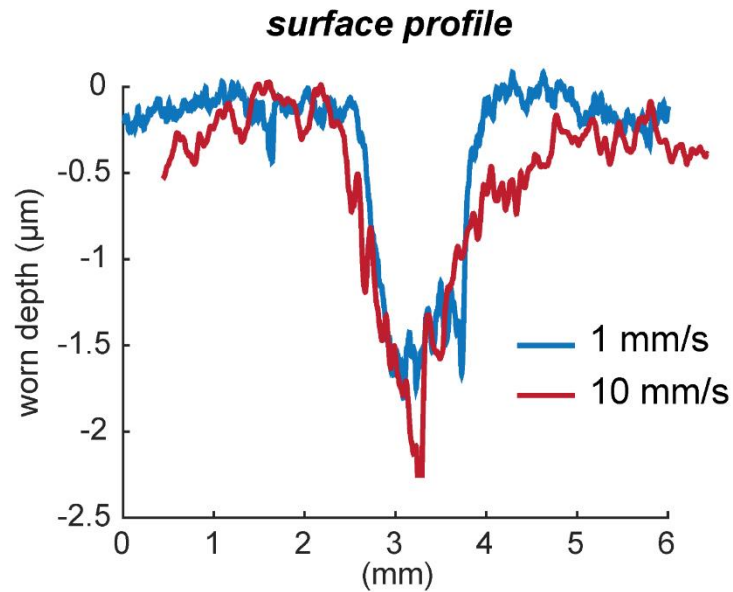
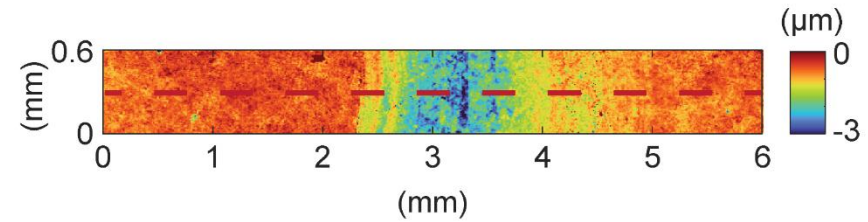
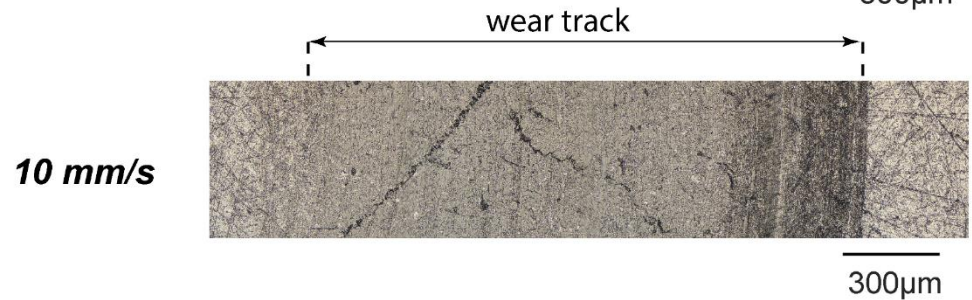
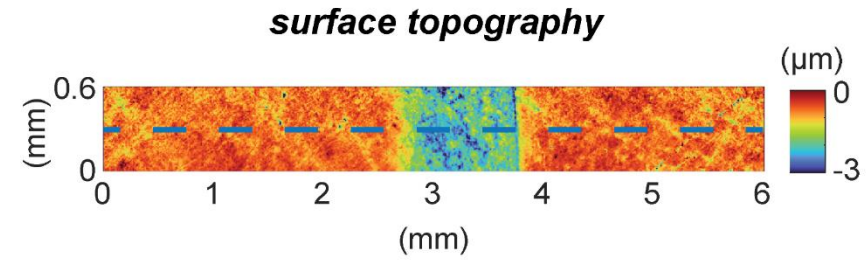
## Furnace





# Wear rate of graphite disk in dry argon

Environment: dry argon    Temperature: 650°C    Normal load: 20 N



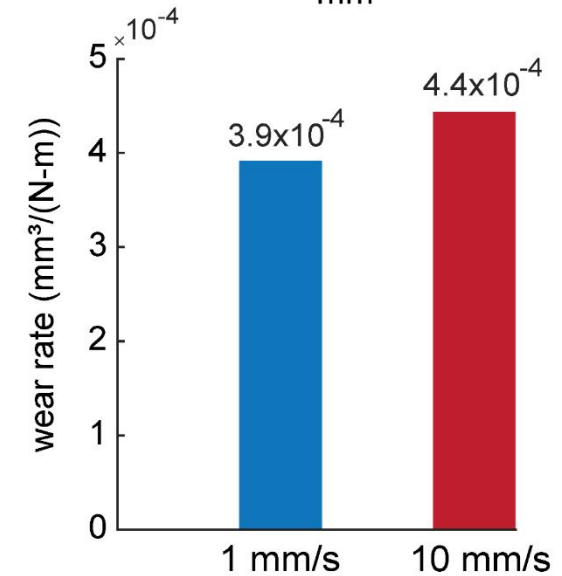
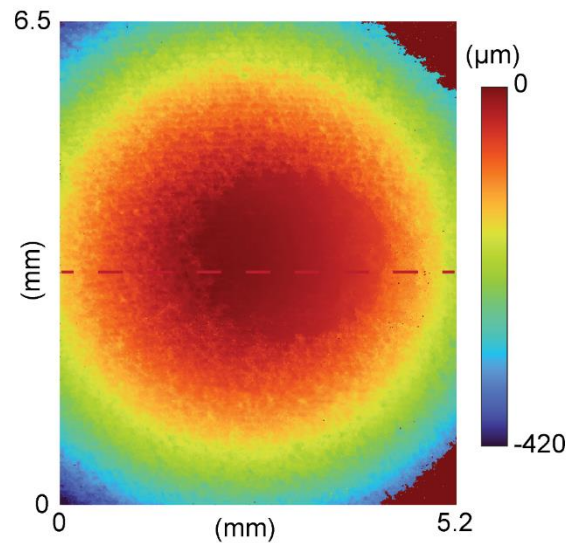
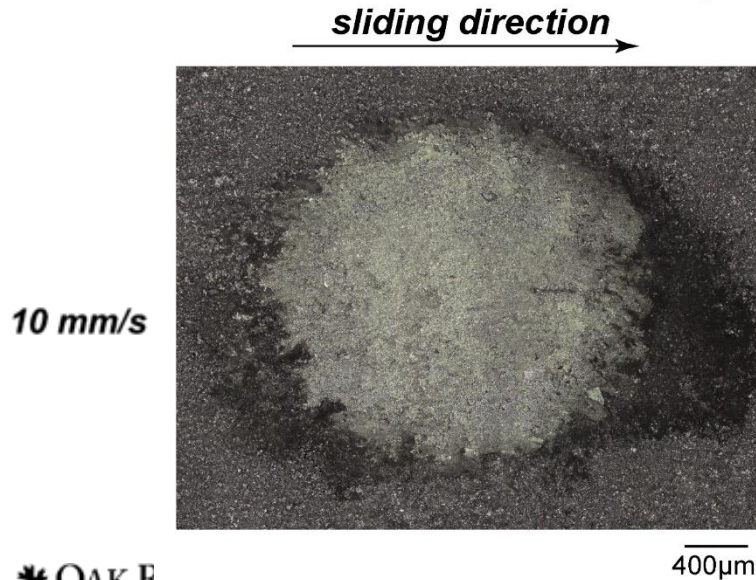
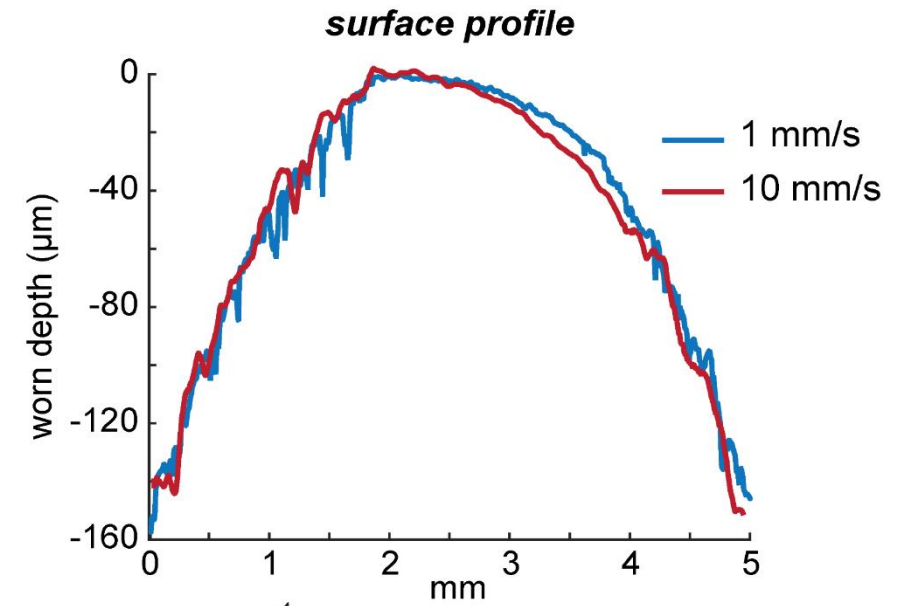
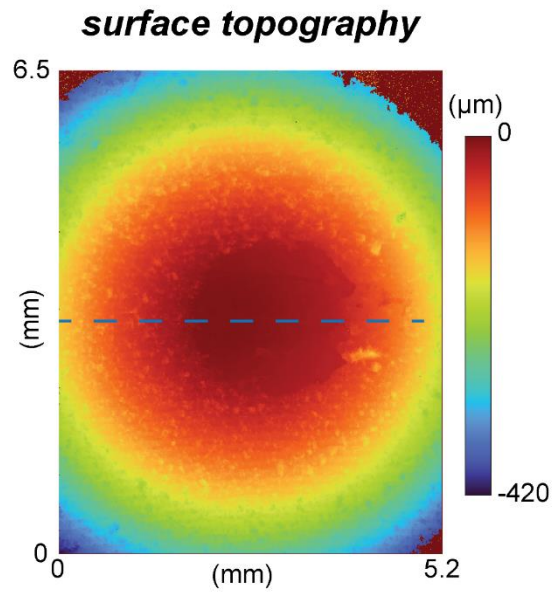
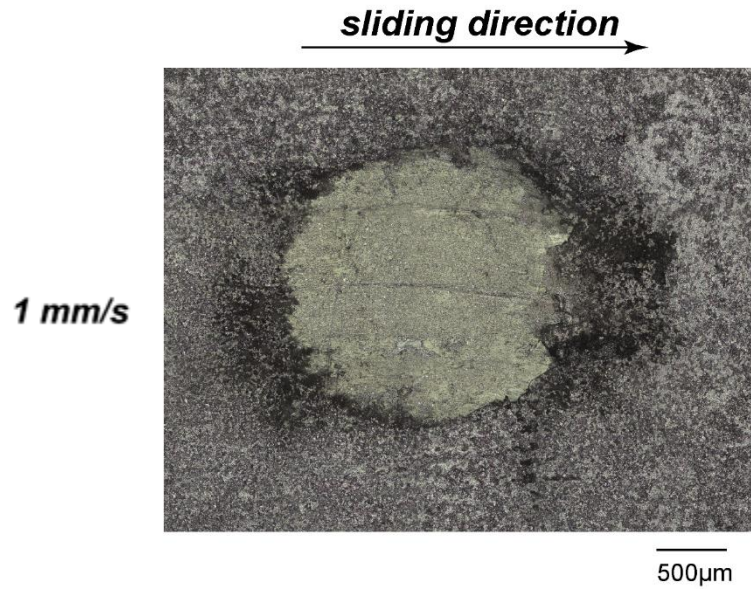
Similar wear rates at 1 and 10 mm/s speeds.

# Wear rate of graphite pin in dry argon

Environment: dry argon

Temperature: 650°C

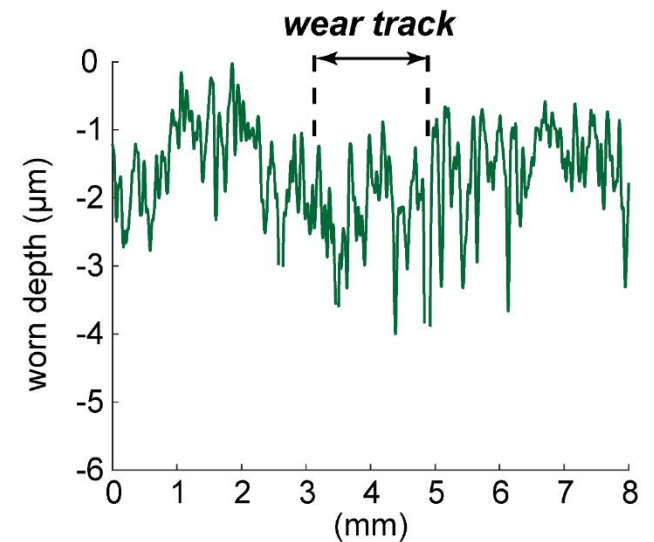
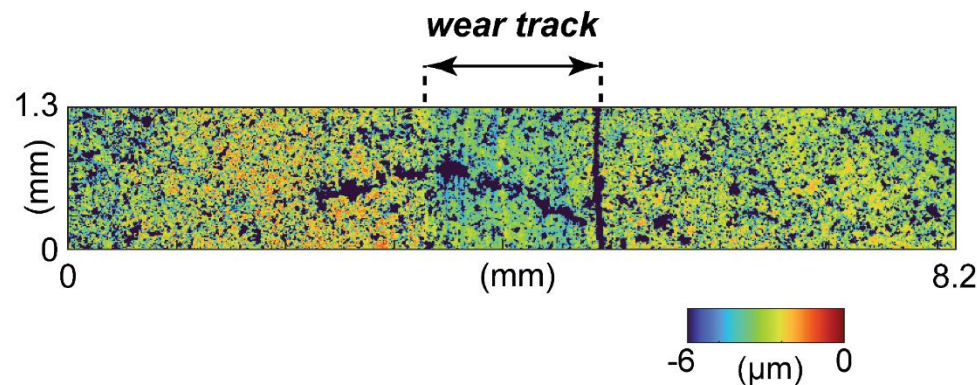
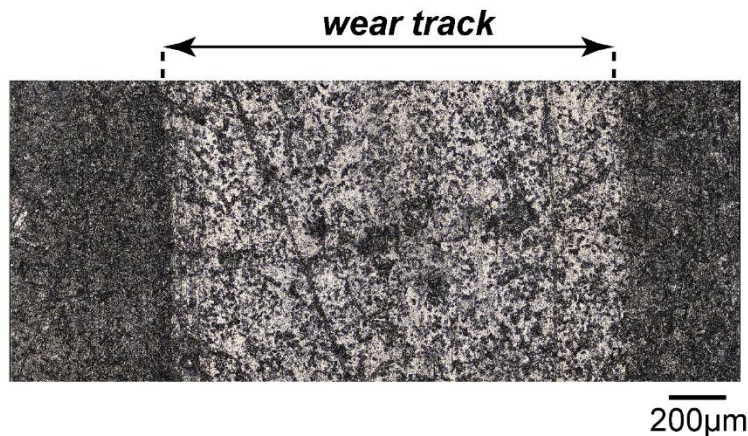
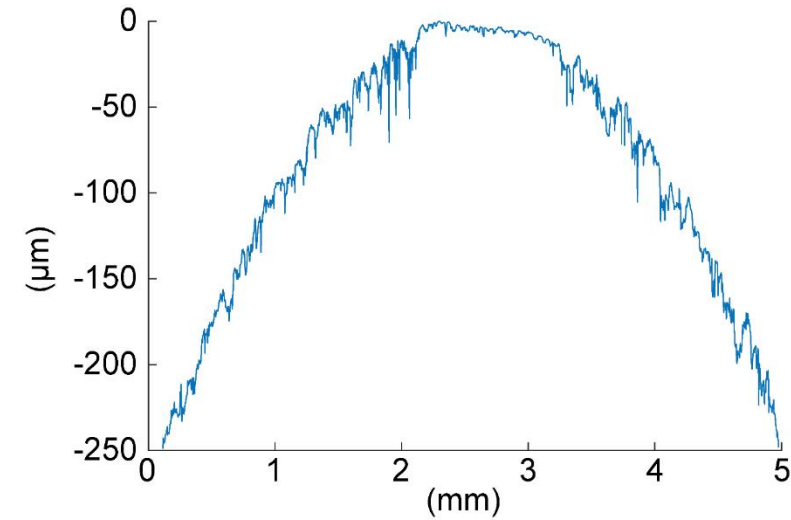
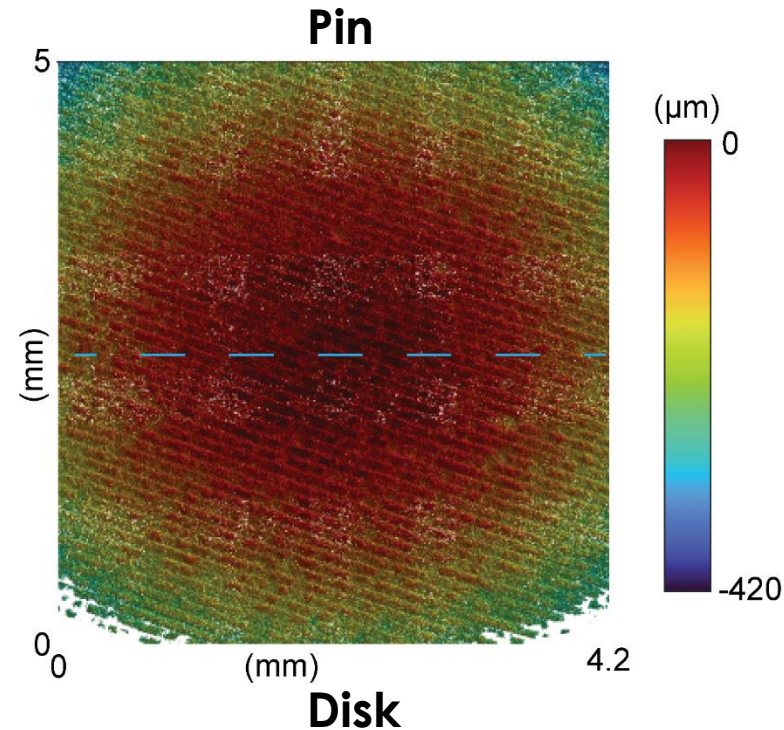
Normal load: 20 N





# Wear rate of graphite pin & disk in molten FLiNaK salt

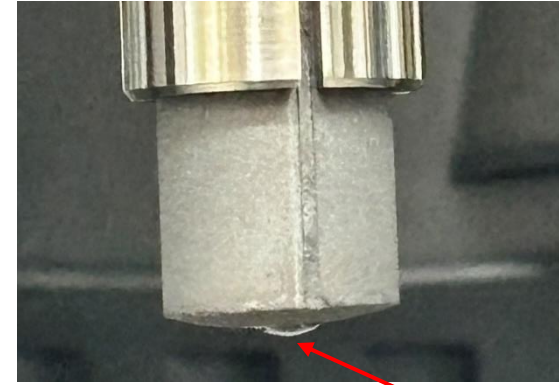
**Environment:** molten FLiNaK salt    **Temperature:** 650°C    **Normal load:** 20 N





# Challenges: removing salt from graphite surface

- Salt remains on the graphite surface as a residue.
- Salt needs to be dissolved by sonicating in DI water.
- Dissolving and sonicating salt from the graphite surface can prevent investigation of key morphological and chemical alterations of the sliding surface.



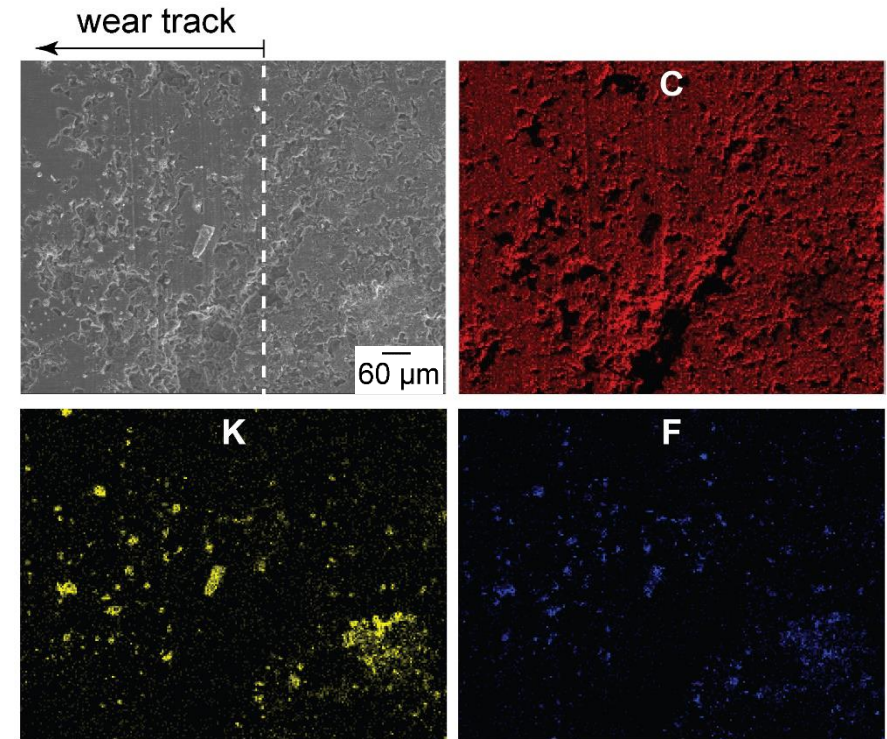
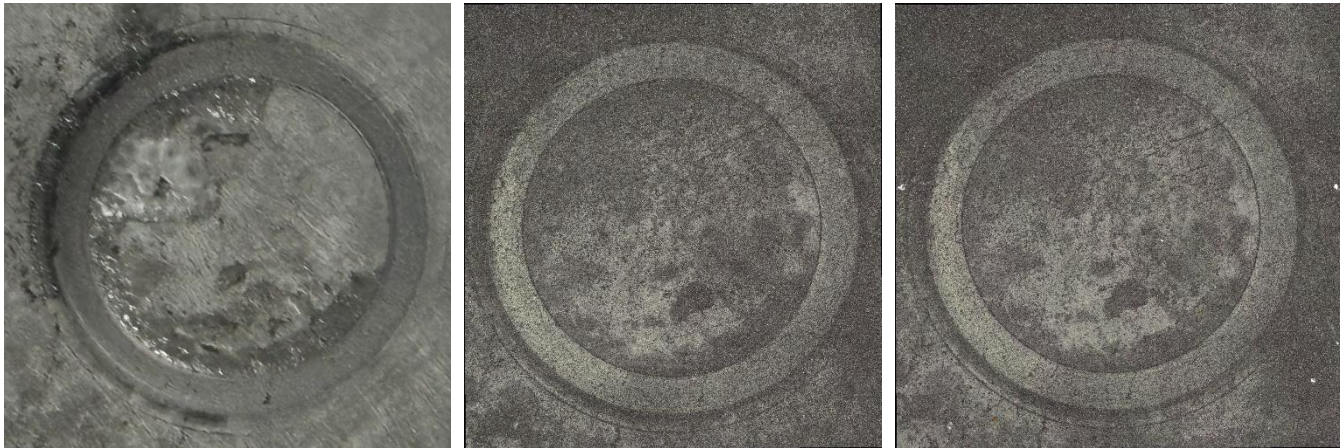
salt residue

## Sonication time

1 hour

2 hours

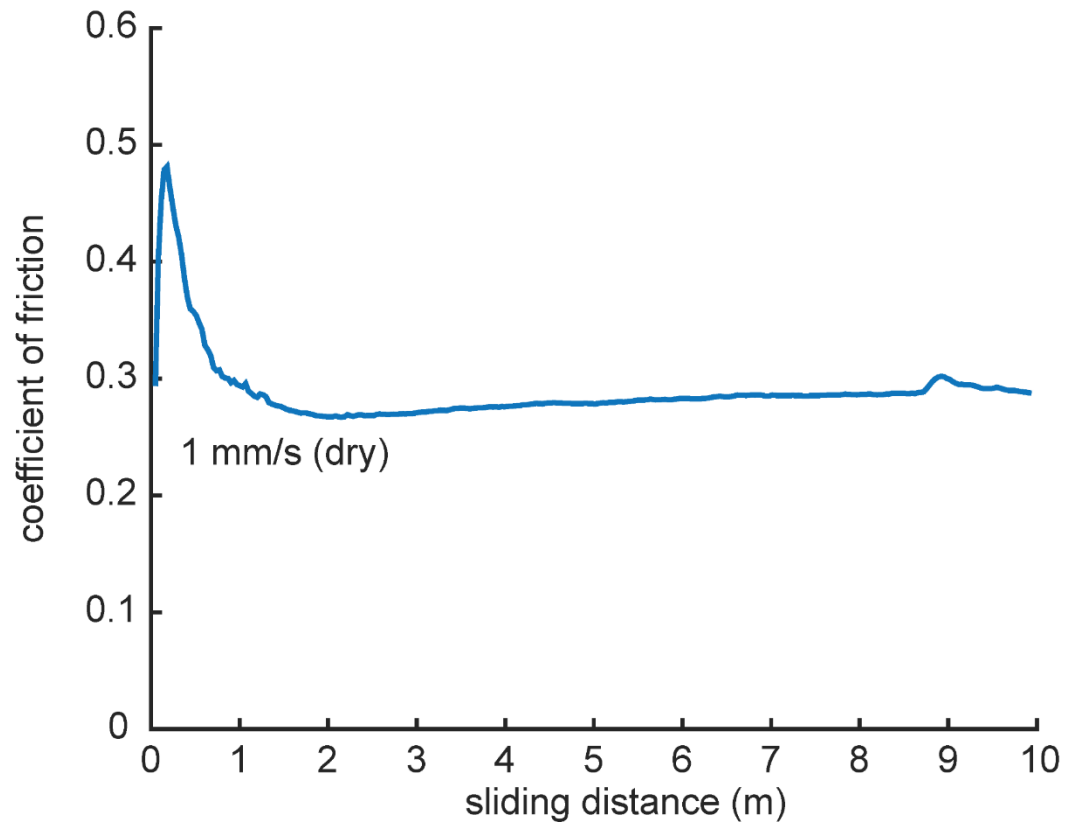
3 hours



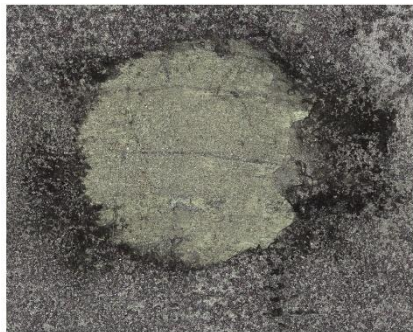
**Salt residues remain on graphite surface after sonication!**



# Friction coefficient



1 mm/s (dry)



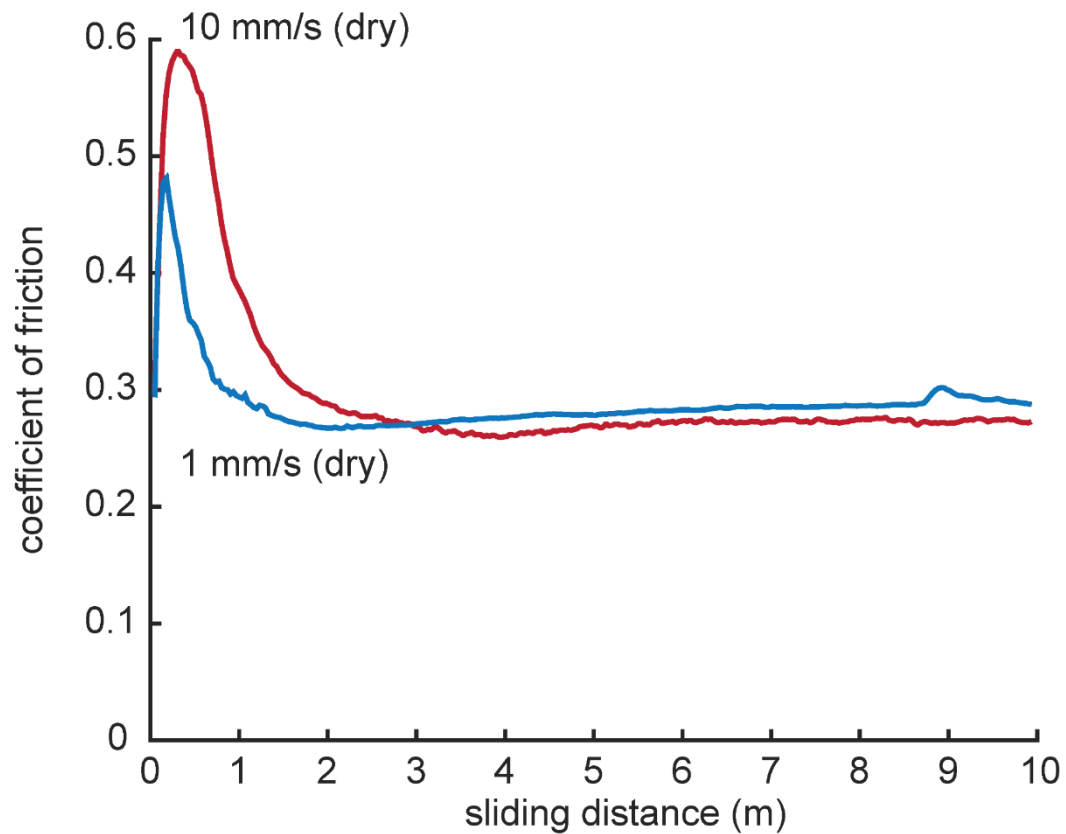
400µm

Temperature=650°C

Load=20 N

Lubrication condition	Sliding speed (mm/s)	Maximum COF	Steady state COF
Dry argon	1	<b>0.47</b>	<b>0.28</b>
Dry argon	10		
Molten FLiNaK Salt	10		

# Friction coefficient

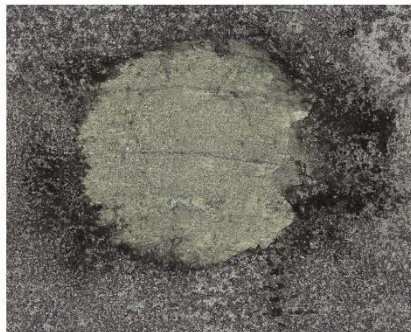


Temperature=650°C      Load=20 N

Lubrication condition	Sliding speed (mm/s)	Maximum COF	Steady state COF
Dry argon	1	<b>0.47</b>	<b>0.28</b>
Dry argon	10	<b>0.58</b>	<b>0.27</b>
Molten FLiNaK Salt	10		

- Higher run-in friction at 10 mm/s.
- Similar steady-state friction.

1 mm/s (dry)



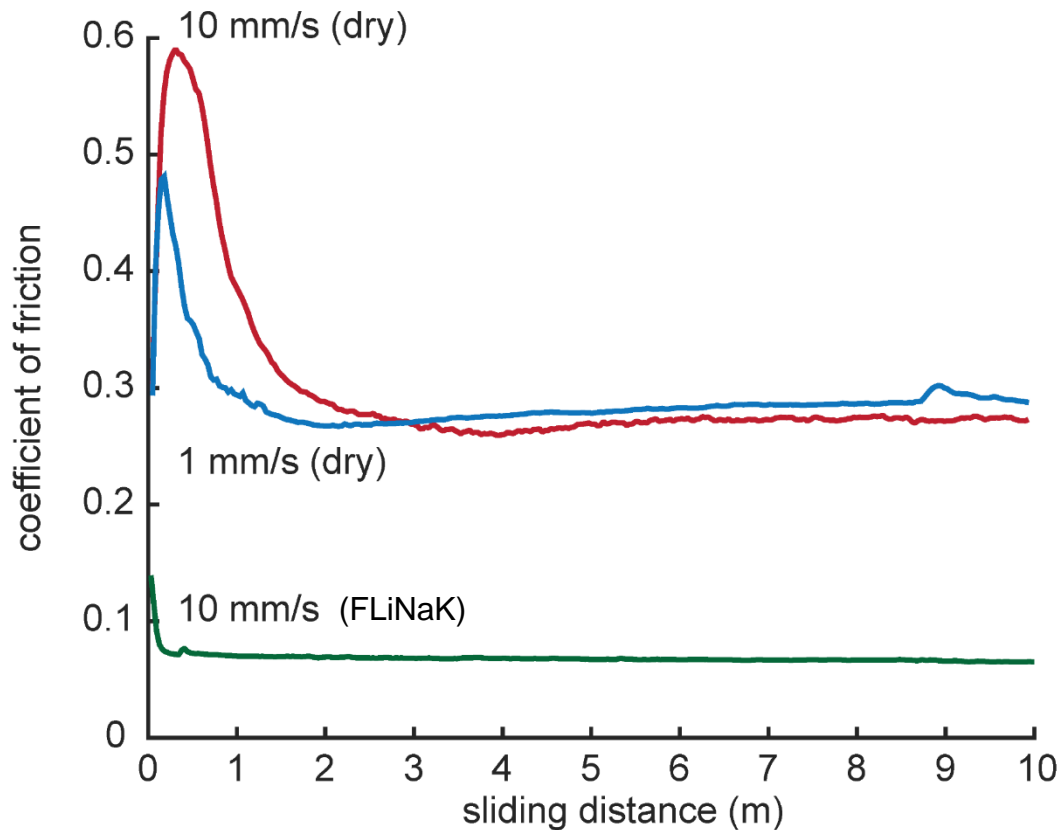
400µm

10 mm/s (dry)



400µm

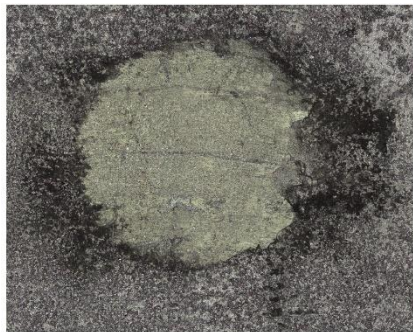
# Friction coefficient



Temperature=650°C      Load=20 N

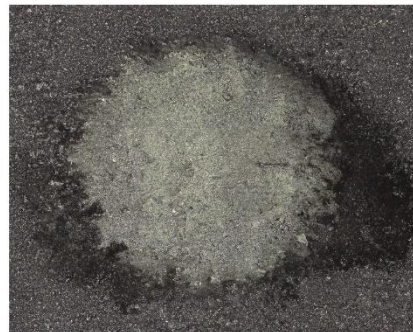
Lubrication condition	Sliding speed (mm/s)	Maximum COF	Steady state COF
Dry argon	1	<b>0.47</b>	<b>0.28</b>
Dry argon	10	<b>0.58</b>	<b>0.27</b>
Molten FLiNaK Salt	10	<b>0.14</b>	<b>0.07</b>

1 mm/s (dry)



400µm

10 mm/s (dry)



400µm

10 mm/s (FLiNaK)



400µm

- Higher run-in friction at 10 mm/s.
- Similar steady-state friction.
- **Molten salt significantly reduces friction.**

# Test matrix for upcoming studies

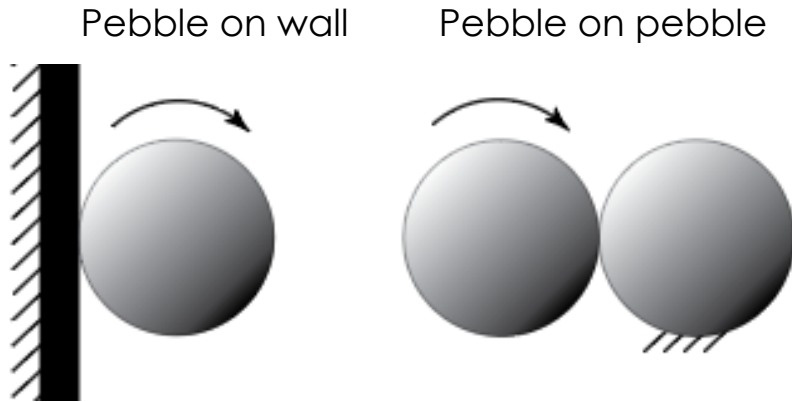
**Environment:** dry argon & molten salt

<b>Force (N)</b>	<b>20</b>		<b>40</b>		<b>80</b>	
<b>Sliding speed (mm/s)</b>	1	10	1	10	1	10
<b>Temperature (°C)</b>	650	650	650	650	650	650
<b>Sliding distance (m)</b>	20	20	20	20	20	20



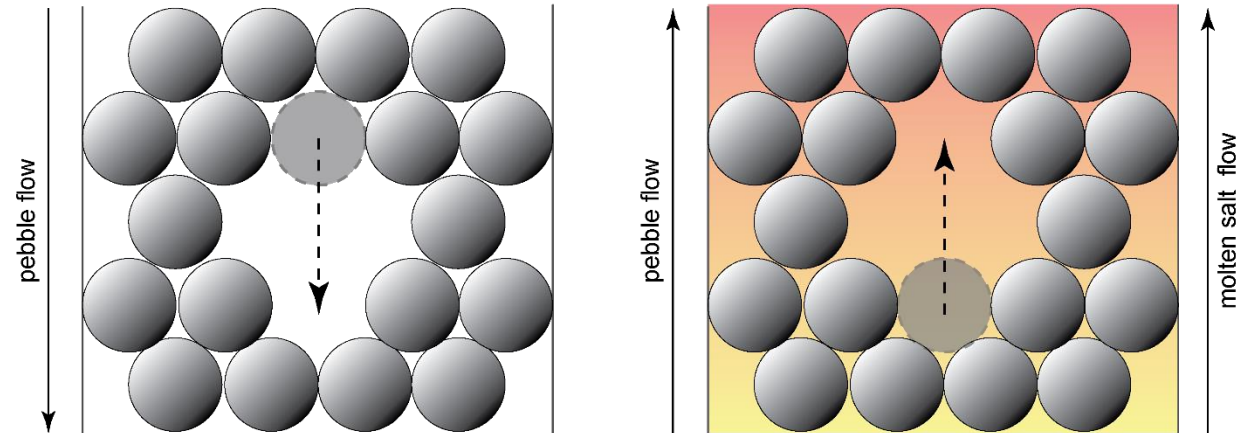
# Topics of Interest (Potential Future Studies)

## Rolling contact



- Pebbles roll against other pebbles and the graphite wall during circulation in the reactor.
- Designing rolling test at high temperatures could be challenging.

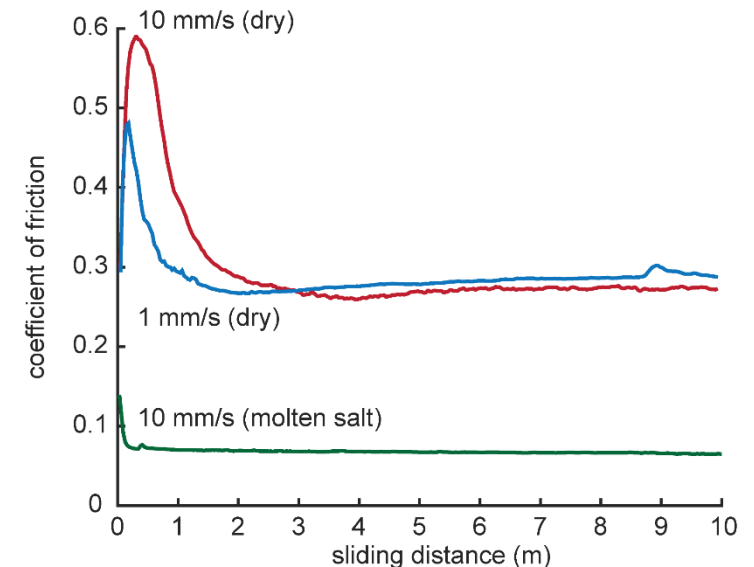
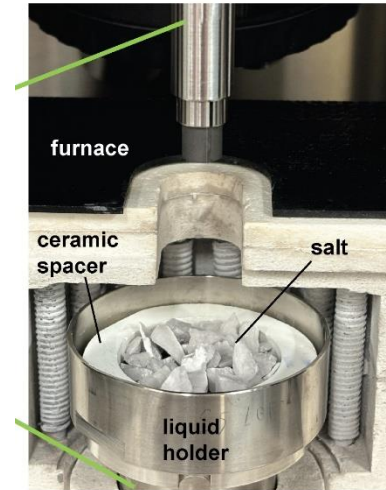
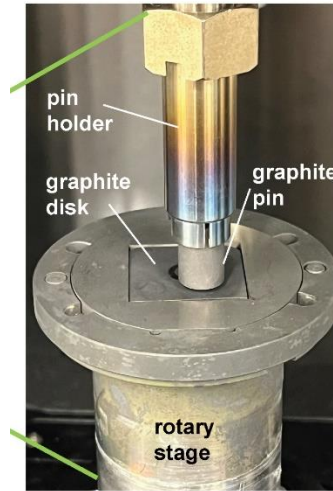
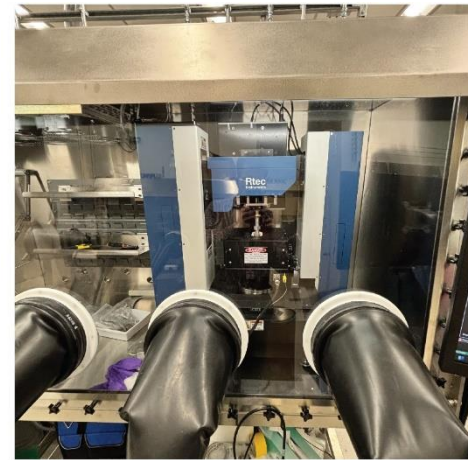
## Impact contact



- Pebbles are not uniformly distributed and there could be voids in the pebble bed matrix.
- A pebble could move through the void and collide with an opposing pebble.
- This would cause an impact contact – higher contact loads and speeds.

# Conclusions and acknowledgements

- Developed capabilities to characterize the tribological properties of graphite in dry argon and molten salt environments at high temperatures.
- Determined the tribologically relevant conditions in gas-cooled and molten salt reactors.
- Identified challenges and limitations of tribological testing with molten salts.
- Performed initial studied tribological studies of graphite in dry argon and molten salt environment.



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