



**GAS-COOLED REACTOR**

ADVANCED REACTOR TECHNOLOGIES PROGRAM

7-16-2024

# Thermophysical Property Characterization of Irradiated TRISO Compacts

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**DOE ART GCR Review Meeting**

*Hybrid Meeting at INL*

**July 16–18, 2024**

# Research Group & Contributors

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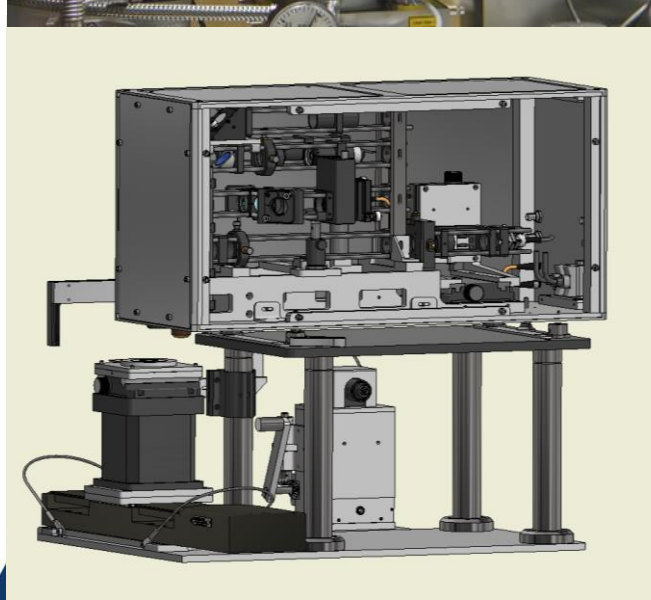
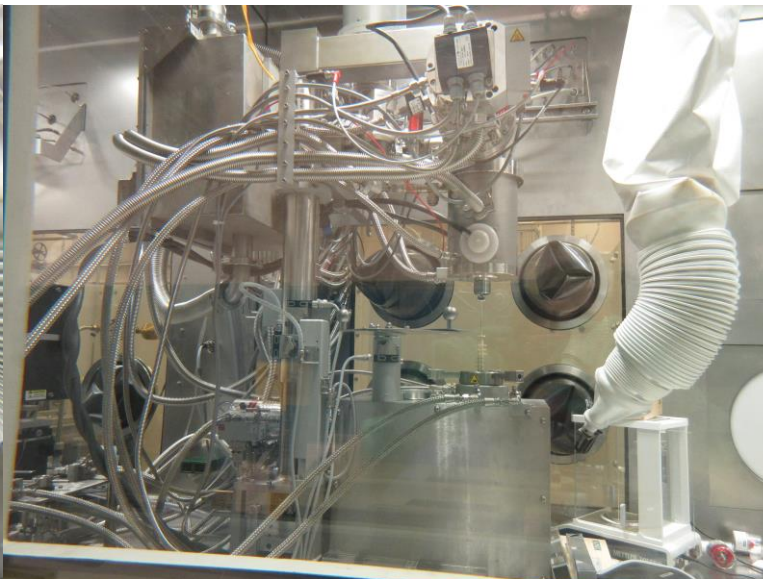
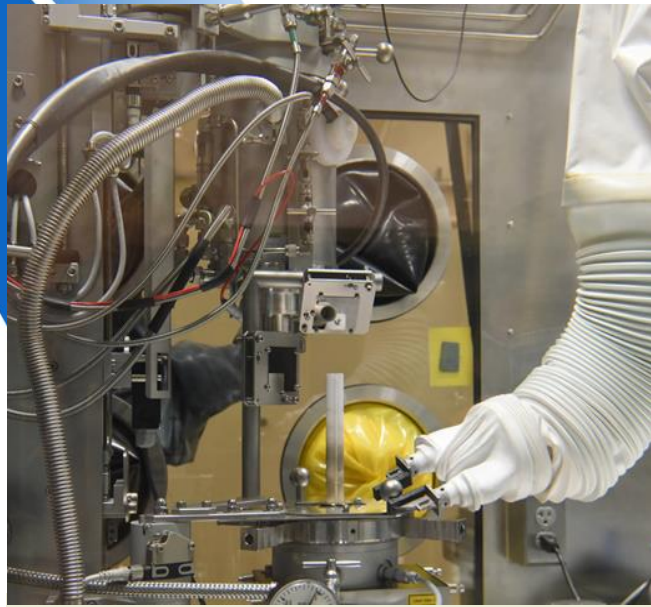
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**Special thanks to IMCL operations staff for their support**



# Overview

- Motivation
- Experiment Background
- TCM Experimental Method
- TCM Results
- Summary and Conclusions
- Future/Ongoing Work



*Top Left: LFA at IMCL, Top Right, STA at IMCL  
Bottom Left: TCM diagram, Bottom Right, TCM at IMCL*

# Motivation

- Measurements of thermophysical properties are used in thermomechanical fuel performance code to model the performance of reactors in normal and abnormal conditions
- The temperature across the fuel specimen (governed by thermophysical properties) in a nuclear reactor will affect:
  - mechanical properties
  - Fission product/gas transport and release
  - Fuel compact pressurization (stress states of the fuel, layers, and matrix)
- This work provides first-of-a-kind PIE on mesoscale thermal transport data for TRISO particles
  - A novel thermophysical properties source for fuel performance codes
  - Will contribute to an understanding of the microstructural evolution of TRISO materials thermal transport properties from pre- to post-irradiation



# AGR-2 Compacts and Characteristics

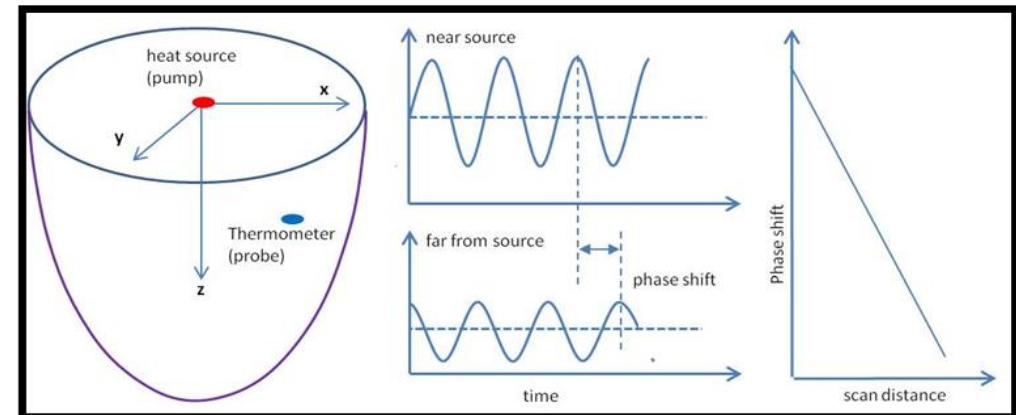
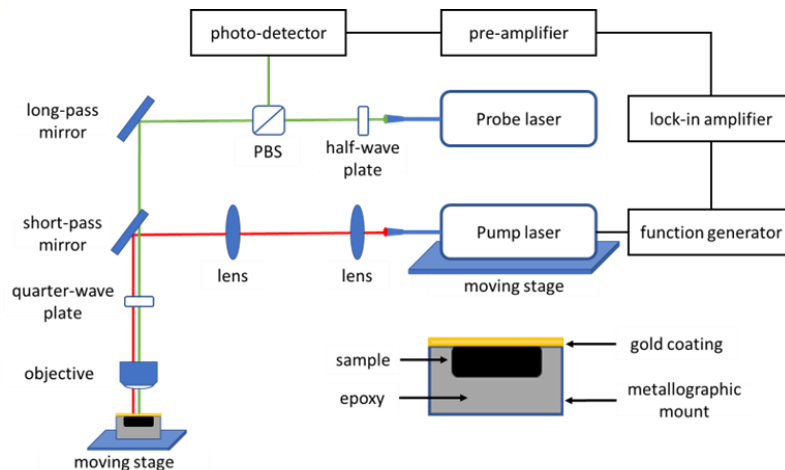
Compact	Sample ID	TAVA Irradiation Temperature (°C)	Burnup (% FIMA)	Fuel Type	Fast Fluence ( $10^{25}$ n/m <sup>2</sup> E>0.18 MeV)	Enrichment (weight % U-235)	Mean Particle Diameter (um)
5-1-3	MNT-64X	1078	11.09	UCO	3.03	14	873
2-4-3	MNT-58X	1216	11.52	UCO	3.08	14	873
2-1-3	MNT-67X	1194	10.95	UCO	2.88	14	873
LEU09-OP2-z	LEU09-F52	NA	NA	UCO	0	14.3	873

- Three samples are from compacts were sourced from the AGR-2 experiment [1]
- One sample consisting of 3 as-fabricated TRISO particles in a surrogate matrix as a baseline [2]

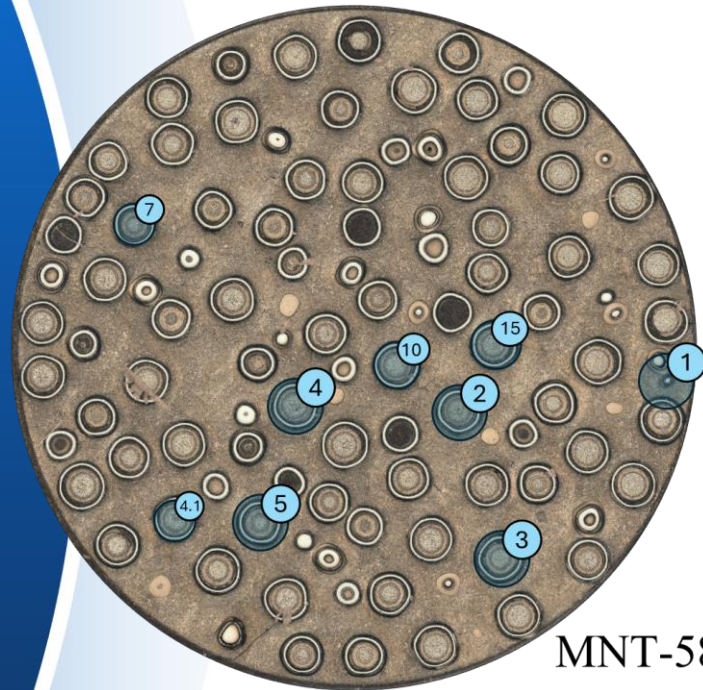


# Thermal Conductivity Microscope (TCM) Methods

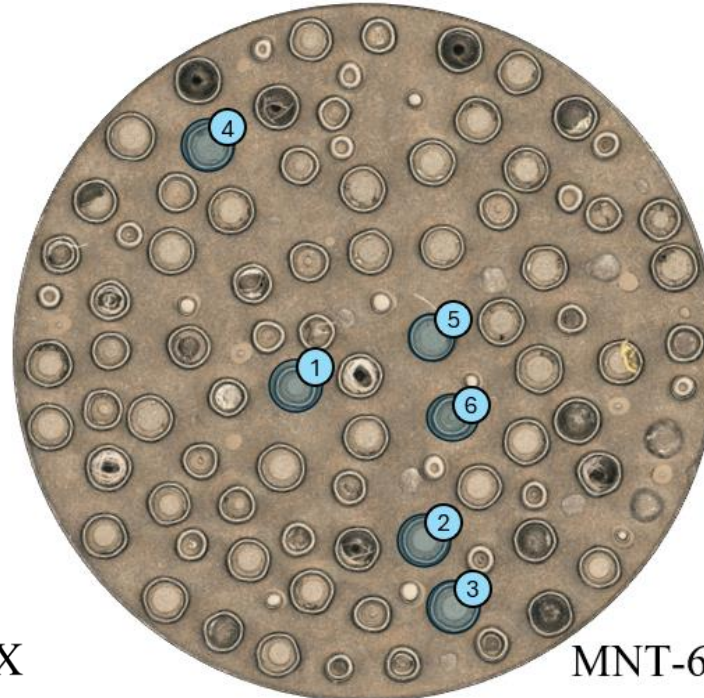
- The TCM is a state-of-the-art instrument built by INL scientists in collaboration with NSUF to deliver a mesoscale thermal transport measurement capability [3].
- The TCM is the only instrument in the world capable of mesoscale thermal transport PIE
- It uses a hybrid thermoreflectance technique to measure thermal conductivity and thermal diffusivity on the microscale ( $\sim 12 - 50 \mu\text{m}$ )
  - Amplitude modulated (1-100 kHz) red heating pump laser generates thermal waves in the substrate
  - A green probe laser, spatially separated from pump laser, measures the effects of changes in optical reflectivity of substrate, mathematically related with heat transport properties of substrate [4].



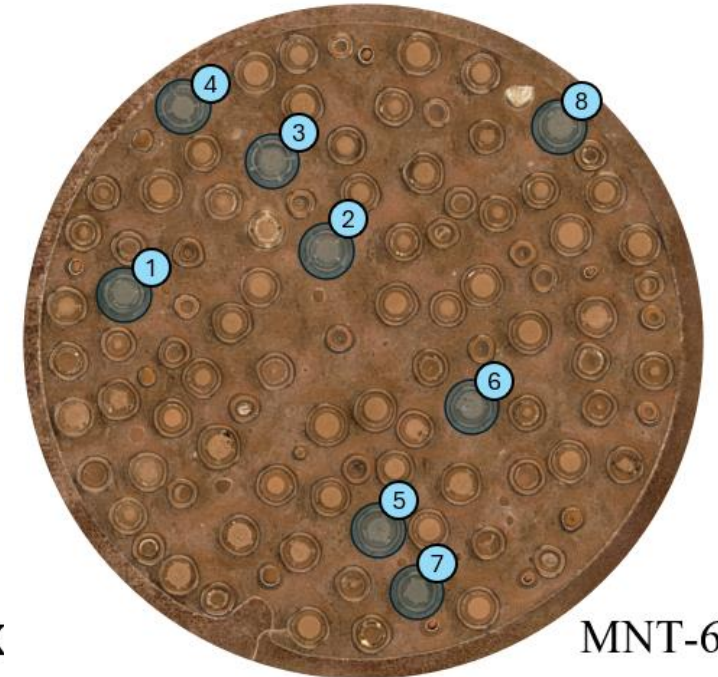
# TCM Particle Selection



MNT-58X



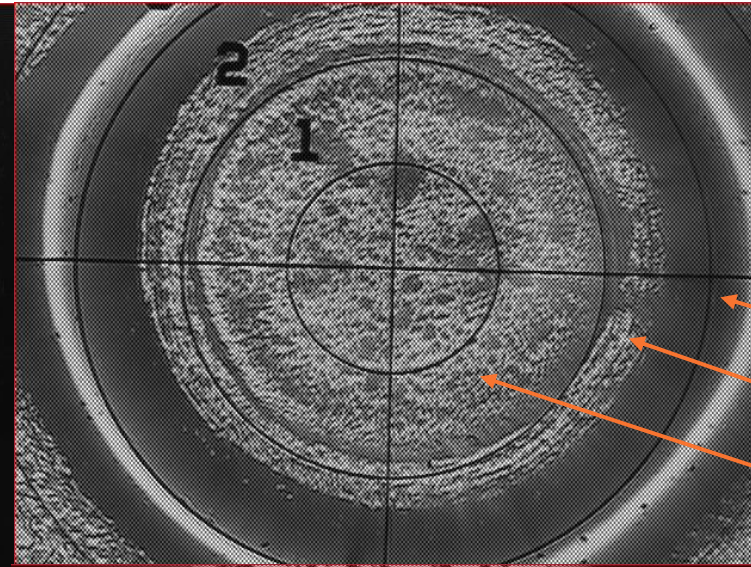
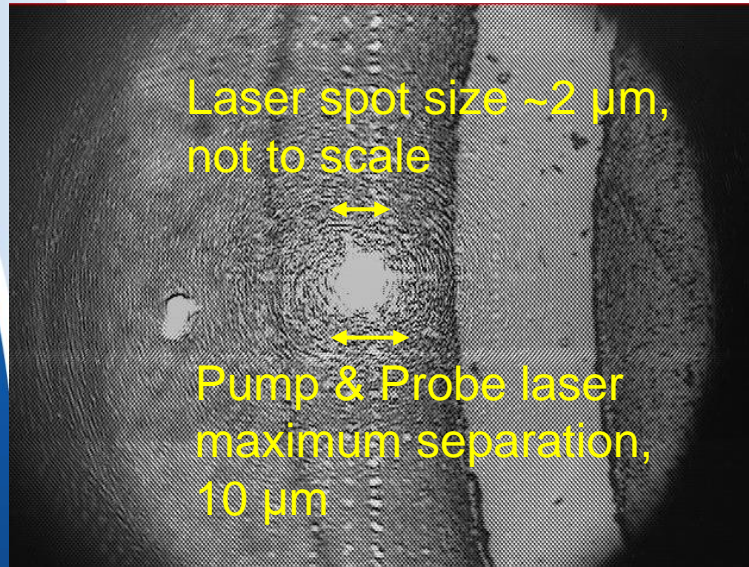
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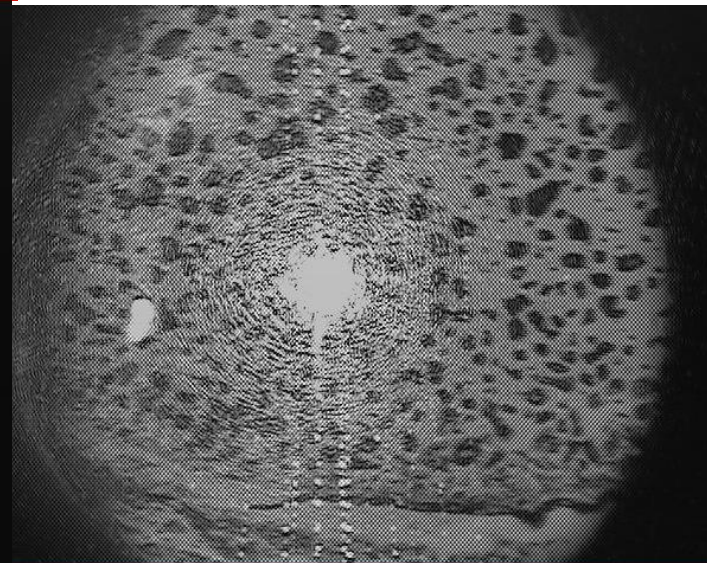
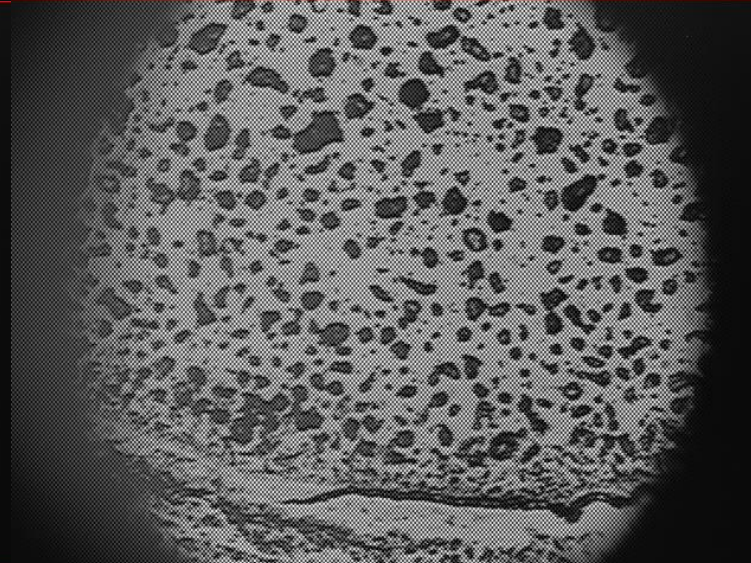
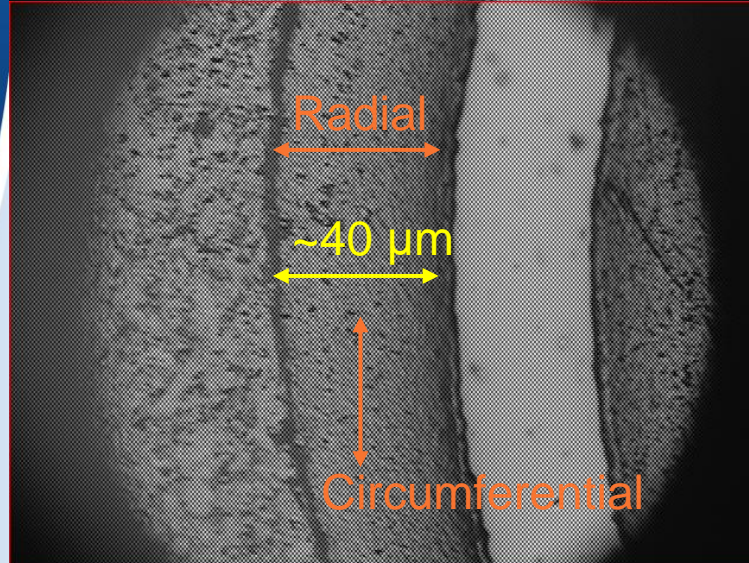
MNT-67X

- Intact, whole particles were chosen for SEM high resolution microscopy and TCM measurements
- Particles were selected based on evaluating effects of radial distance from the center of the compact

# TCM Measurement Examples



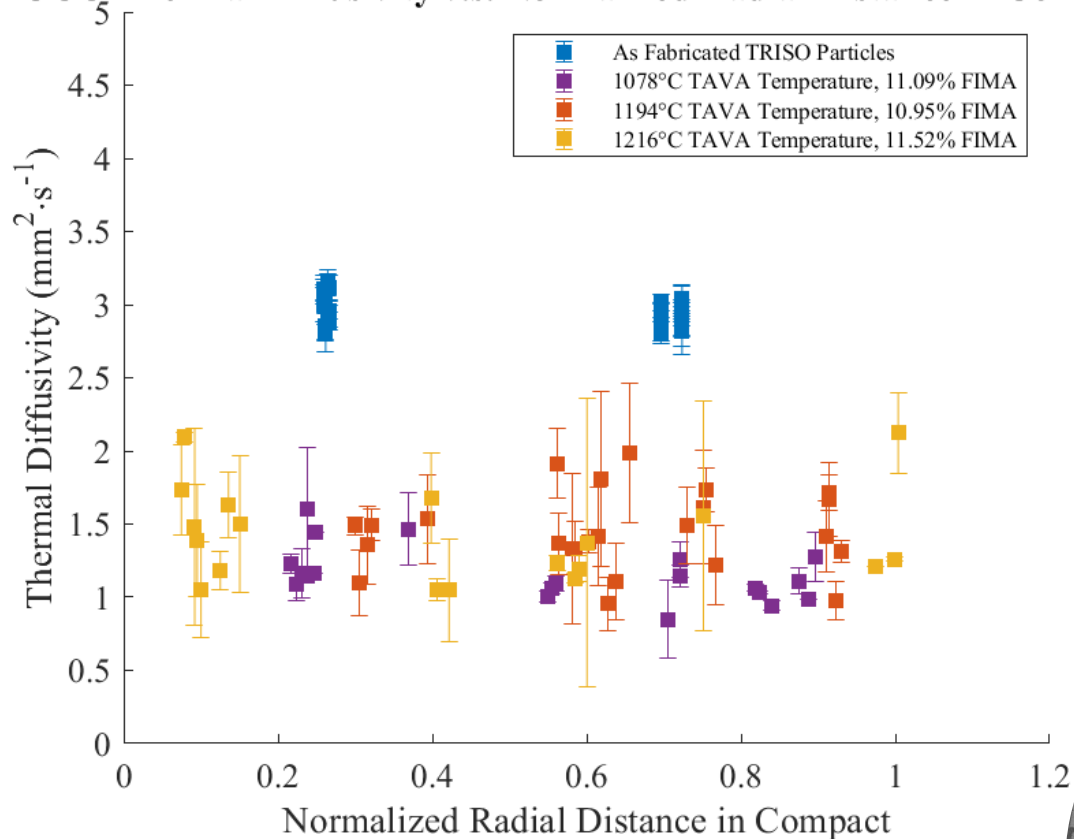
OPyC  
SiC  
IPyC  
Buffer  
Fuel





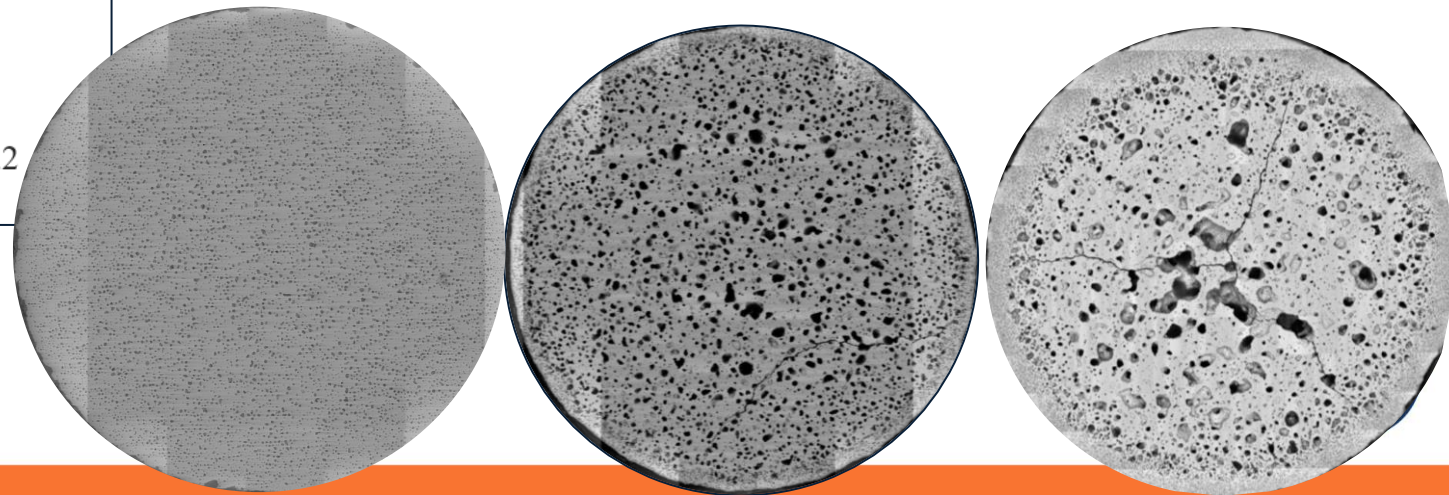
# UCO Kernel Pre- to Post-Irradiation

UCO Thermal Diffusivity v.s. Normalized Radial Distance in Compact



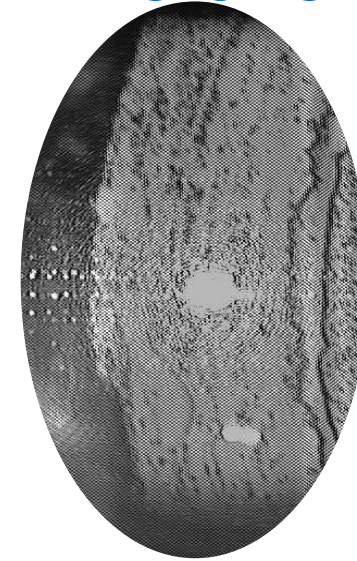
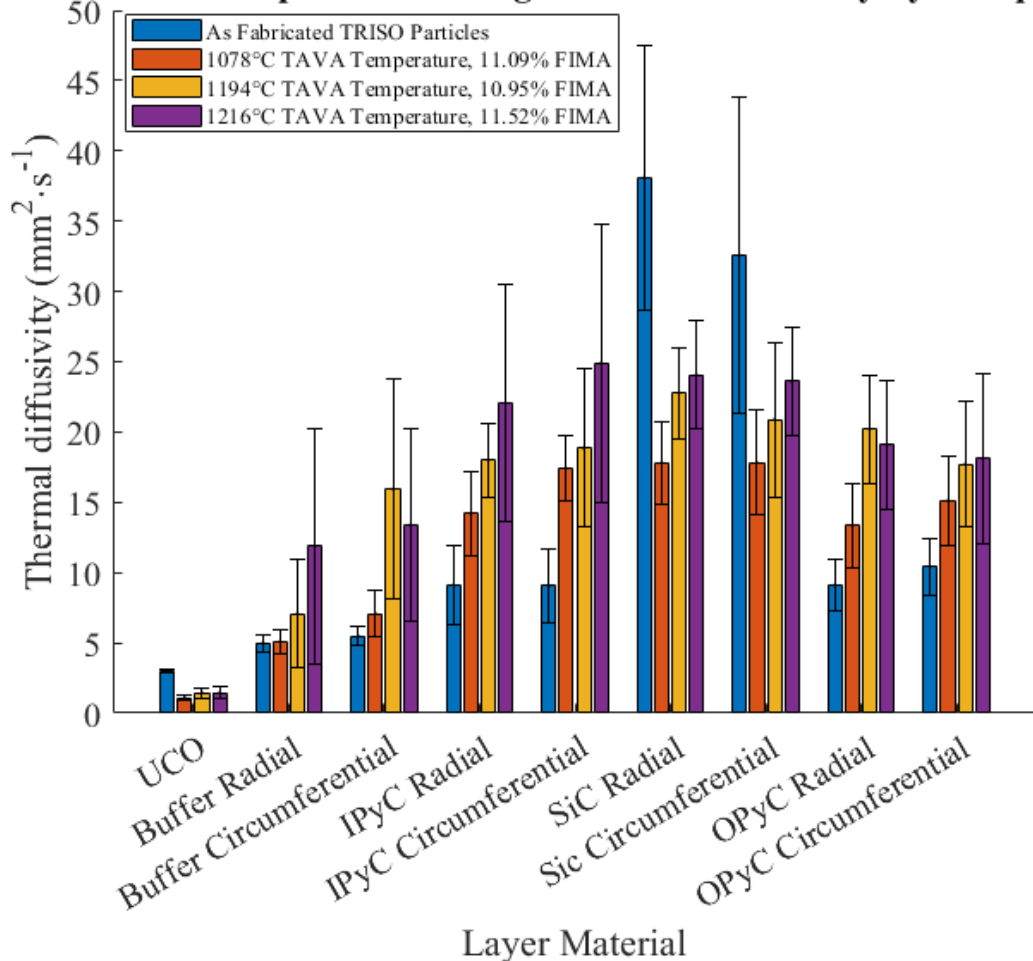
- Compared to as fabricated UCO kernels:
  - Average thermal diffusivity in the higher TAVA temperature compacts is decreased by ~50%
  - Average thermal diffusivity in the lower TAVA temperature compacts is decreased by ~64%
- At higher TAVA temperature UCO kernel thermal diffusivity may recover slightly
- Porosity profiles will be needed to better understand degradation of thermal diffusivity and conductivity [5]

TCM Measured fuel particle SEM images by TAVA temperature  
Left to Right: 1078°C, 1194°C, 1216°C



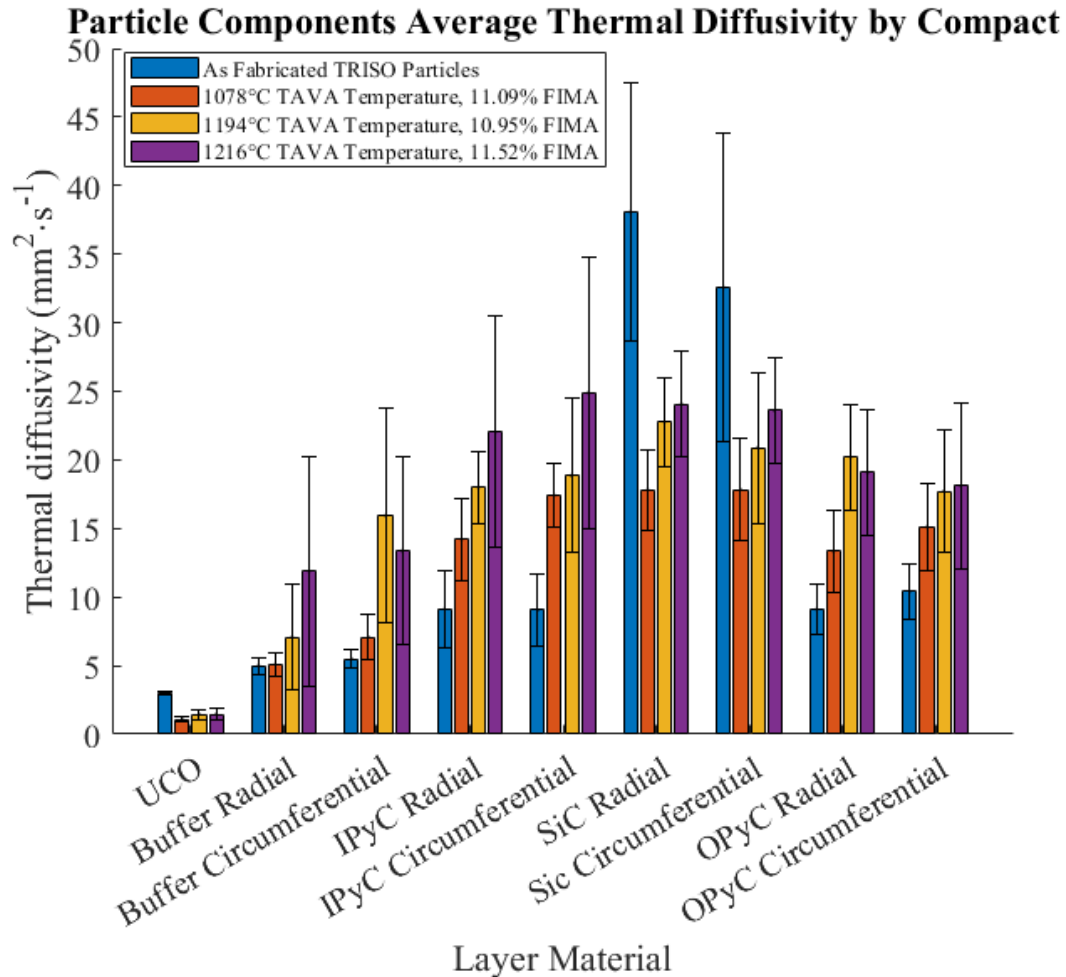
# Buffer Layer Pre- to Post-Irradiation

Particle Components Average Thermal Diffusivity by Compact



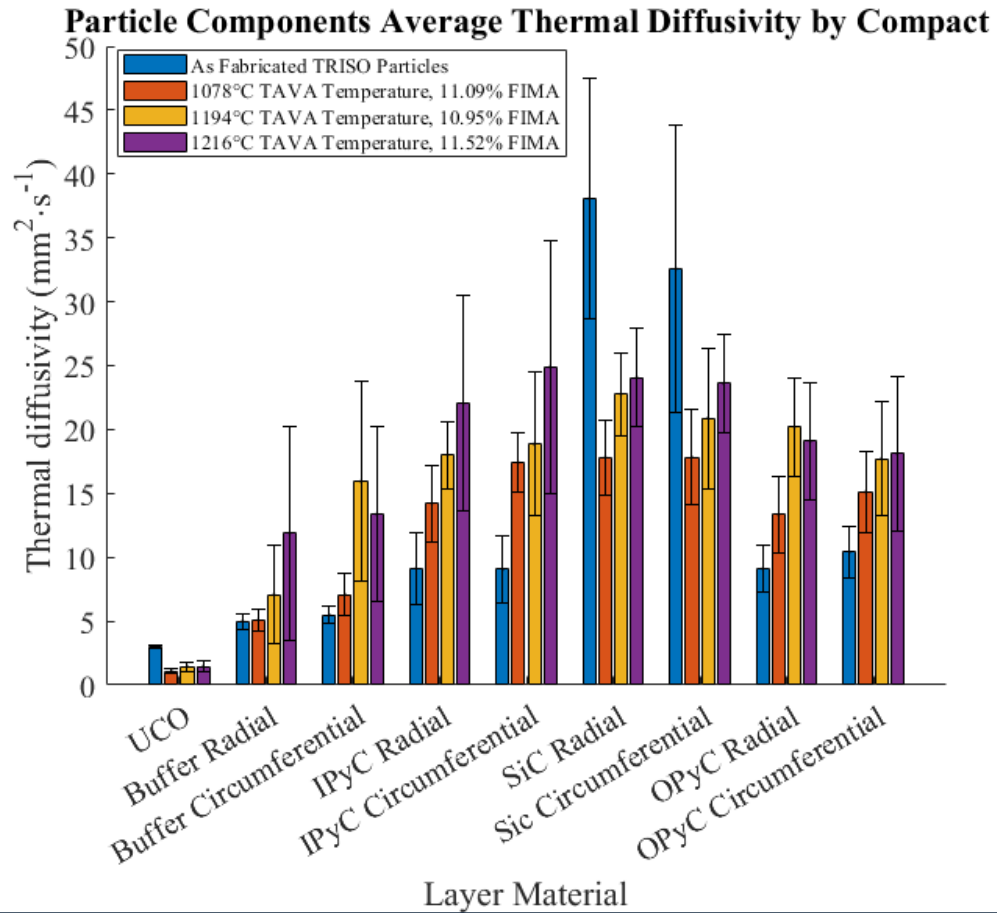
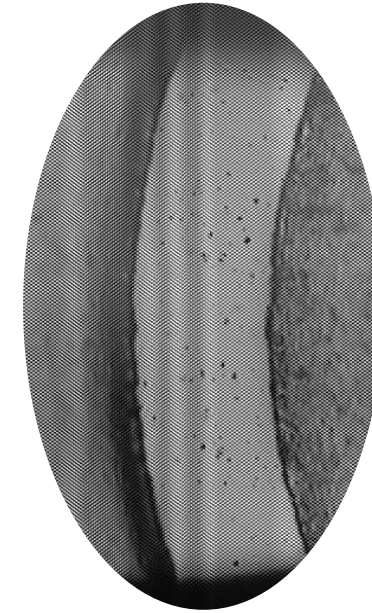
- Thermal diffusivity tends to increase post-irradiation with increases correlated with TAVA temperature
- Likely driven by:
  - Densification of the layer
  - Simultaneous point defect annealing at higher temperatures
- Significant anisotropy is difficult to detect given high deviation from particle to particle
  - Deviation from particle to particle may be due to localized annealing
  - Fabrication defects could also cause variation [6].

# Pyrolytic Carbon Layers Pre- to Post-Irradiation



- Thermal diffusivity increases post-irradiation
  - Potentially due to annealing of fabrication induced defects
- Higher TAVA temperature leads to a higher thermal diffusivity due to annealing of irradiation induced defects
- Difficult to detect any significant anisotropy

# Silicon Carbide Layer Pre- to Post-Irradiation



- Strong degradation from pre- to post-irradiation in thermal diffusivity
  - Irradiation leads to point defects which reduce thermal diffusivity
- Higher TAVA temperatures lead to higher thermal diffusivity values due to annealing of irradiation induced defects
- Potentially other effects contributing to degradation include:
  - Nanovoids [7]
  - Lower thermal conductivity precipitates (e.g. silicides)

# TCM Measurements Conclusions

- Compared to as fabricated material:
  - Fuel and Silicon Carbide thermal diffusivity degrades significantly (50 – 60% and 37 – 53% respectively)
    - Some recovery in thermal diffusivity likely due to annealing at higher TAVA temperatures
  - Pyrolytic Carbons increase thermal diffusivity (ranging from 46 – 175%)
    - Increase correlates to increasing TAVA
- No significant anisotropy found
- Measurements of matrix graphite were attempted with some success, however the surface was non-ideal for TCM measurements
- More than 800 measurements across the 3 compacts



# TCM Measurement Discussion & Takeaways

- Thermal diffusivity values measured by the TCM at RT suggest that PARFUME may be underestimating layer thermal transport (PARFUME's approach is conservative)
- PARFUME values used from 600 to 1300°C [7]:
  - PyC thermal conductivity is assumed to be **invariant** at 4 W/m·K
    - TCM values at RT are between 212% and 712% higher
  - Buffer thermal conductivity is assumed to be **invariant** at 0.5 W/m·K
    - TCM values at RT are between 900% and 1900% higher
  - SiC thermal conductivity is assumed to decrease from 20 to 13 W/m·K
    - TCM values at RT are between 87% and 150% higher
- Annealing of defects in the layers with increasing TAVA temperature may contribute to a higher effective thermal conductivity than currently modeled [8][9].



# Ongoing and Future work at IMCL

- Laser Flash Analysis – high accuracy bulk measurements
  - Custom geometric FEA and EM for heat transfer
  - 1 material property can be extracted using TCM as source for other materials, or whole compact can be compared against TCM
- Simultaneous Thermal Analysis – Differential Scanning Calorimetry
  - Bulk heat capacity
  - Annealing effects
  - Fission gas release
- X-ray Computed Tomography – Search for voids in compacts, establish geometric mesh for EM/FEA modeling for LFA and STA
- Porosity profiles for each TCM measurement for correlation with thermal diffusivity
- Calculation of thermal conductivities using experimental density and heat capacity\*



# Research Group & Contributors

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**Special thanks to IMCL operations staff for their support**





# Questions?

- Additional questions can be sent to:
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  - [Tsvetoslav.pavlov@inl.gov](mailto:Tsvetoslav.pavlov@inl.gov)
  - [John.Stempien@inl.gov](mailto:John.Stempien@inl.gov)



# References

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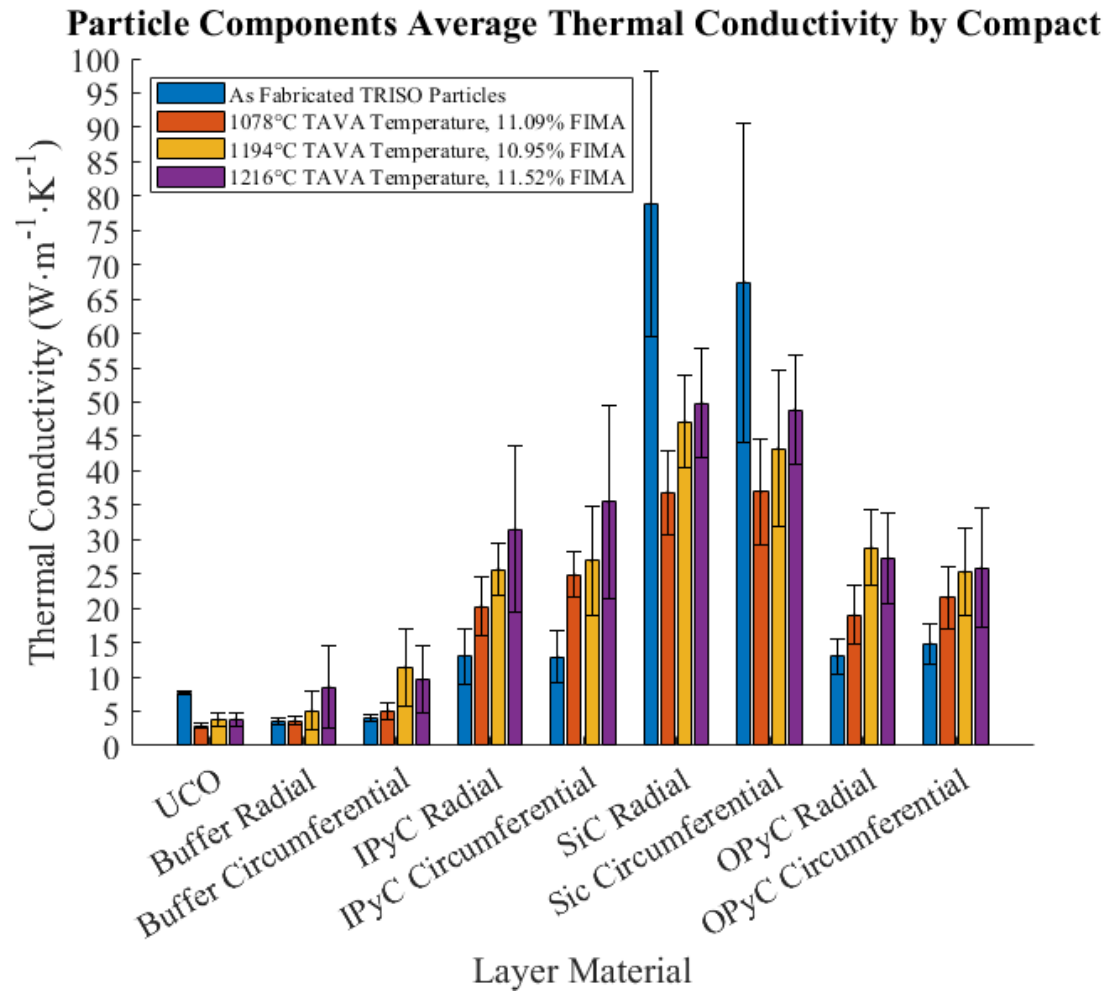


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**ENERGY**

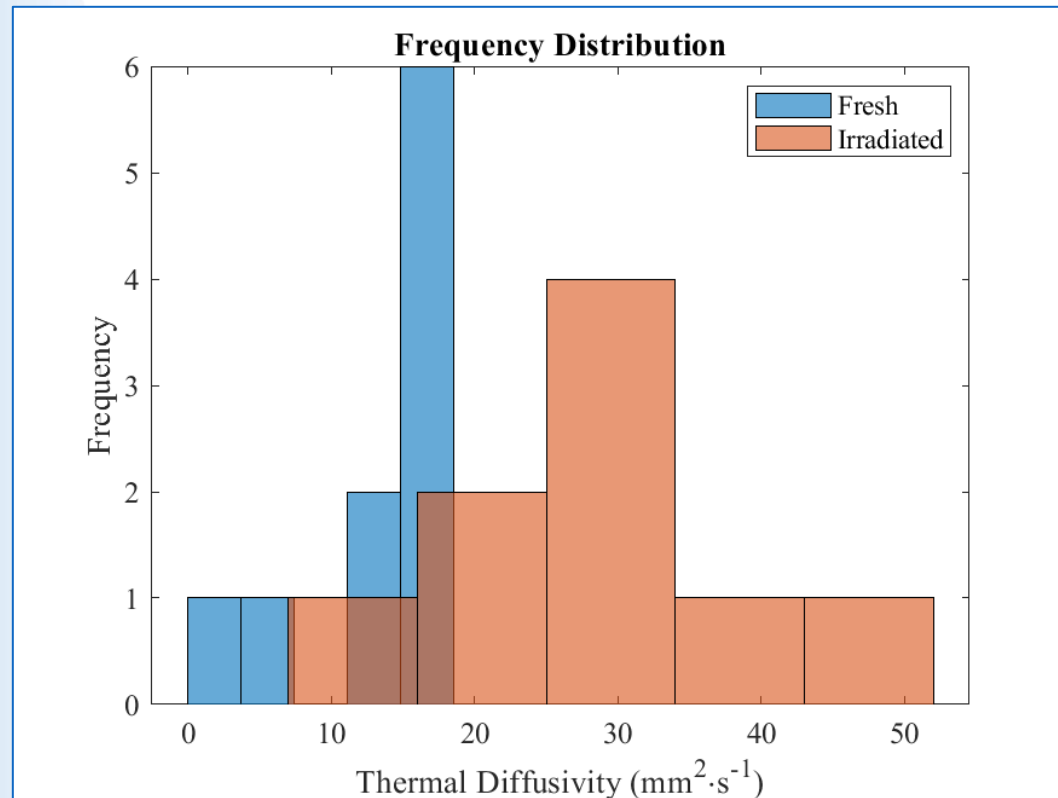
# Supporting Slides



# Thermal Conductivity Calculations



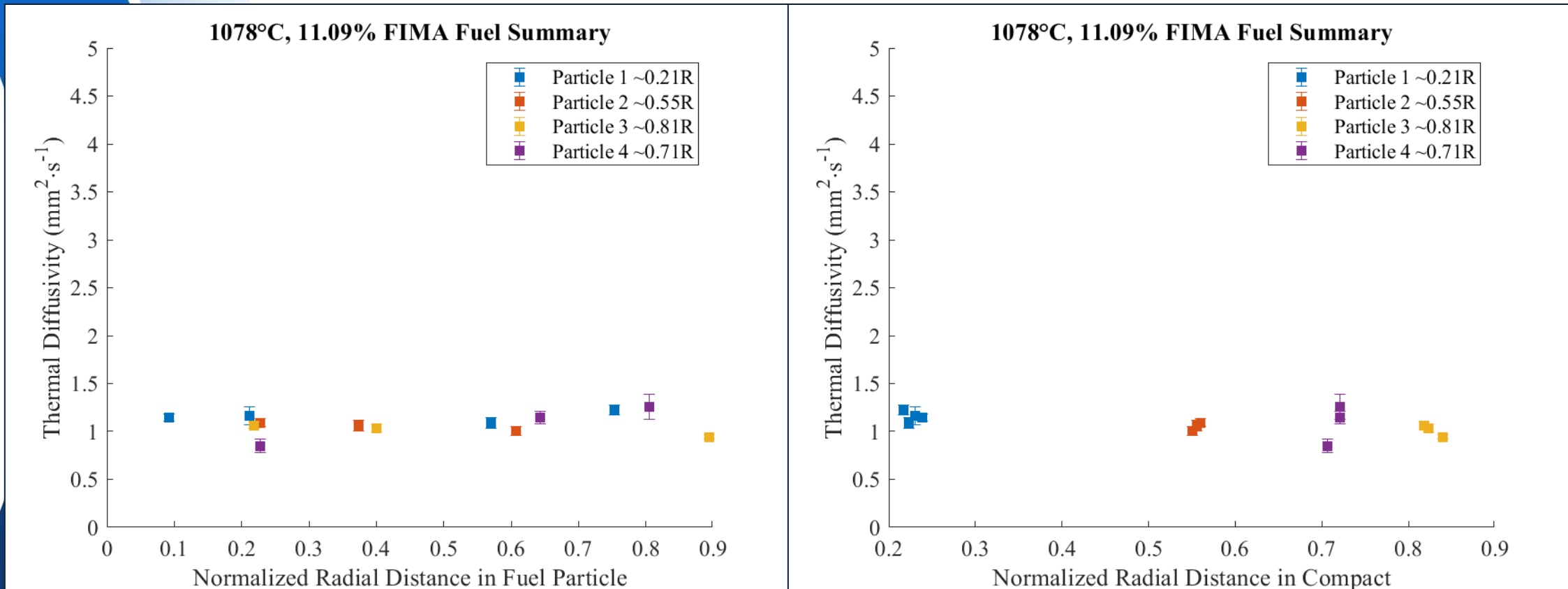
# Graphite Initial Results



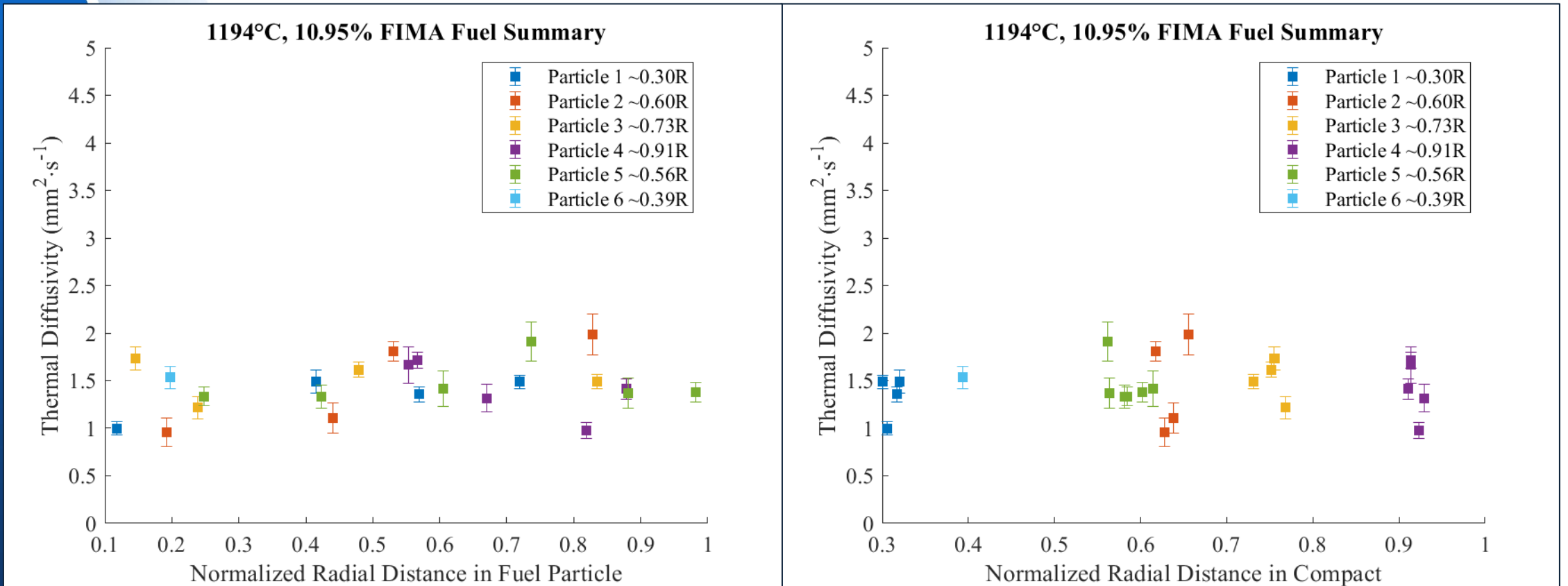
Fresh		Irradiated (1216°C)	
Thermal Diffusivity (mm <sup>2</sup> /s)	Standard Deviation (mm <sup>2</sup> /s)	Thermal Diffusivity (mm <sup>2</sup> /s)	Standard Deviation (mm <sup>2</sup> /s)
13.89	5.38	28.6	9.92



# MNT-64X Fuel Summary

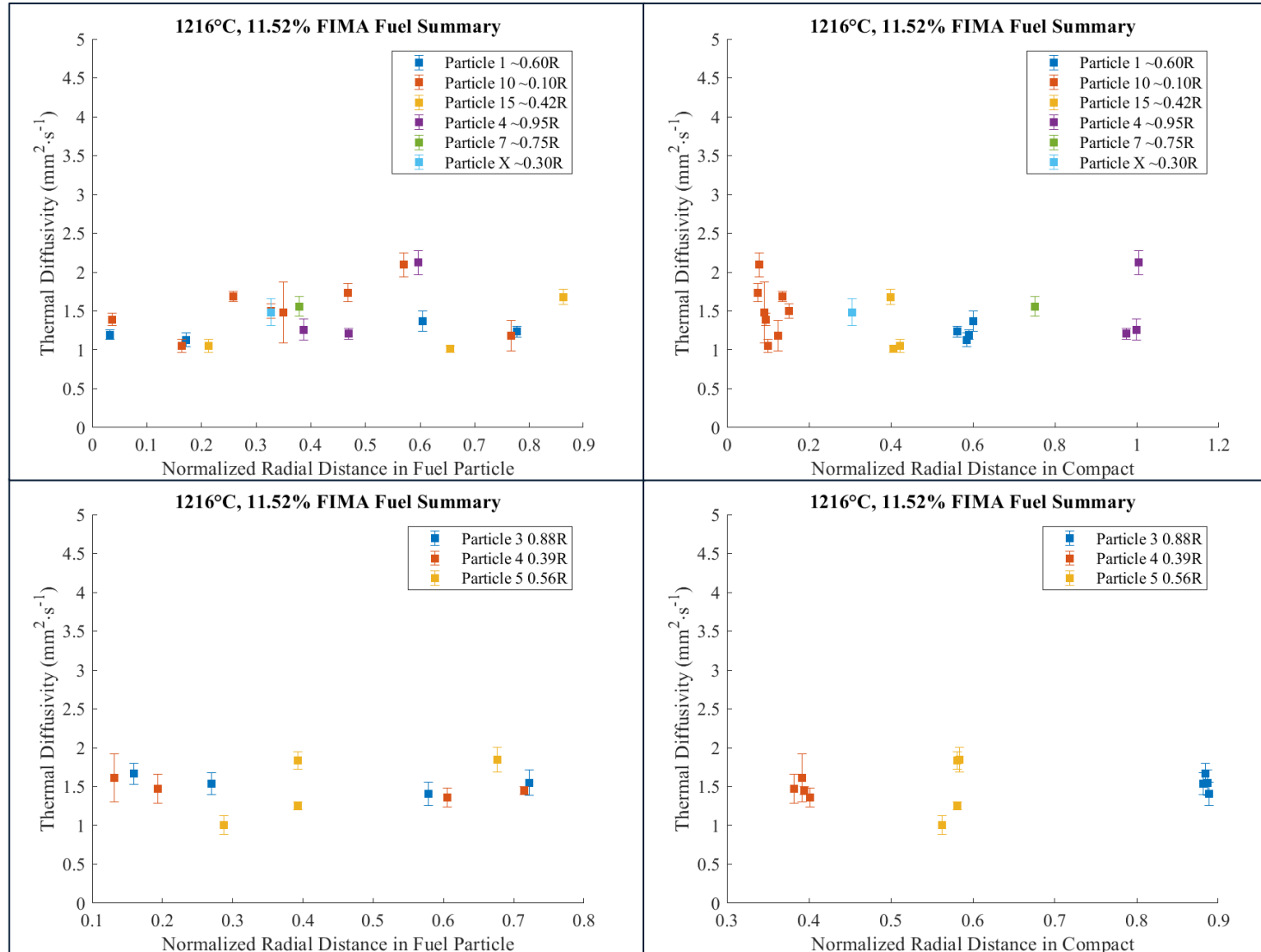


# MNT-67X Fuel Summary

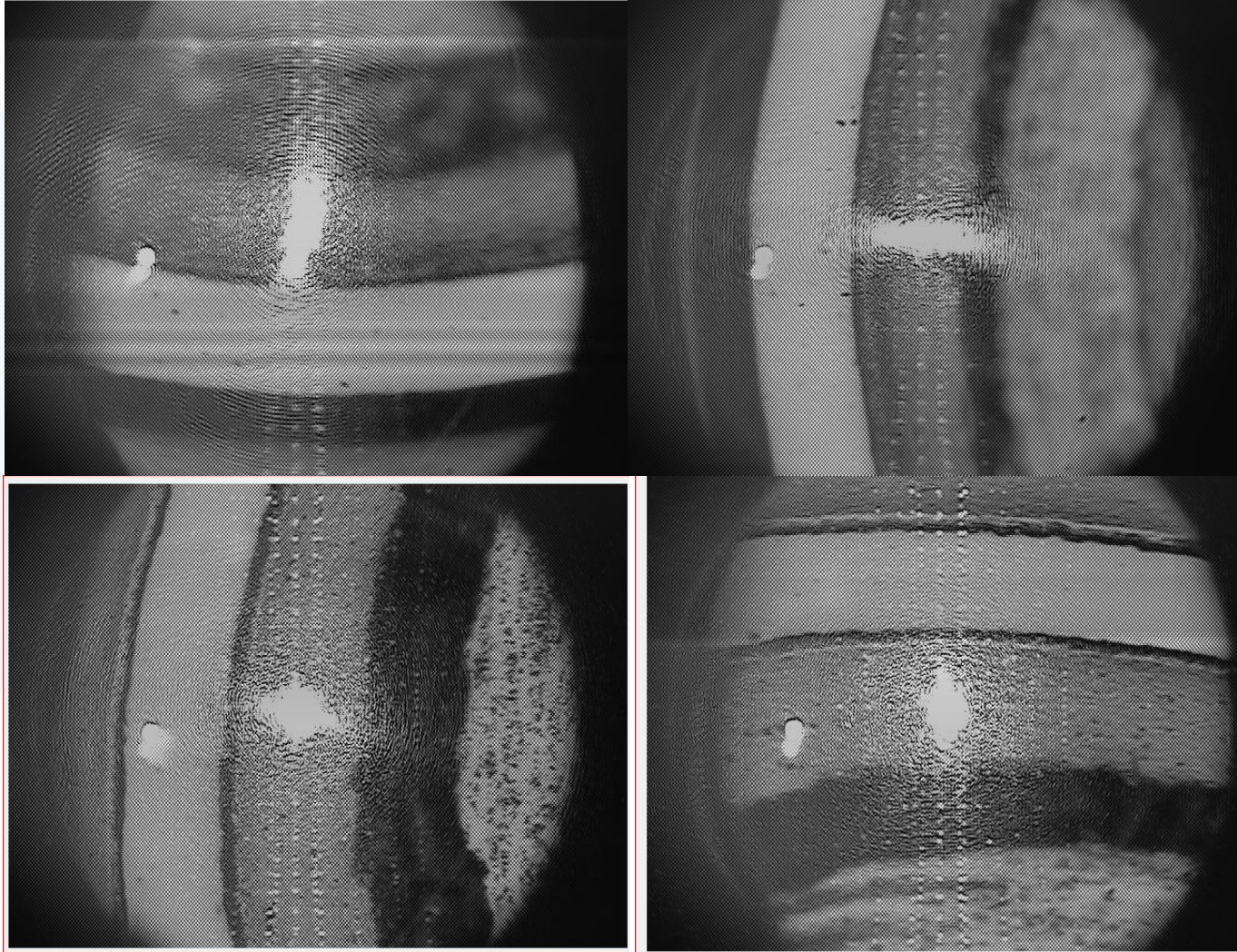




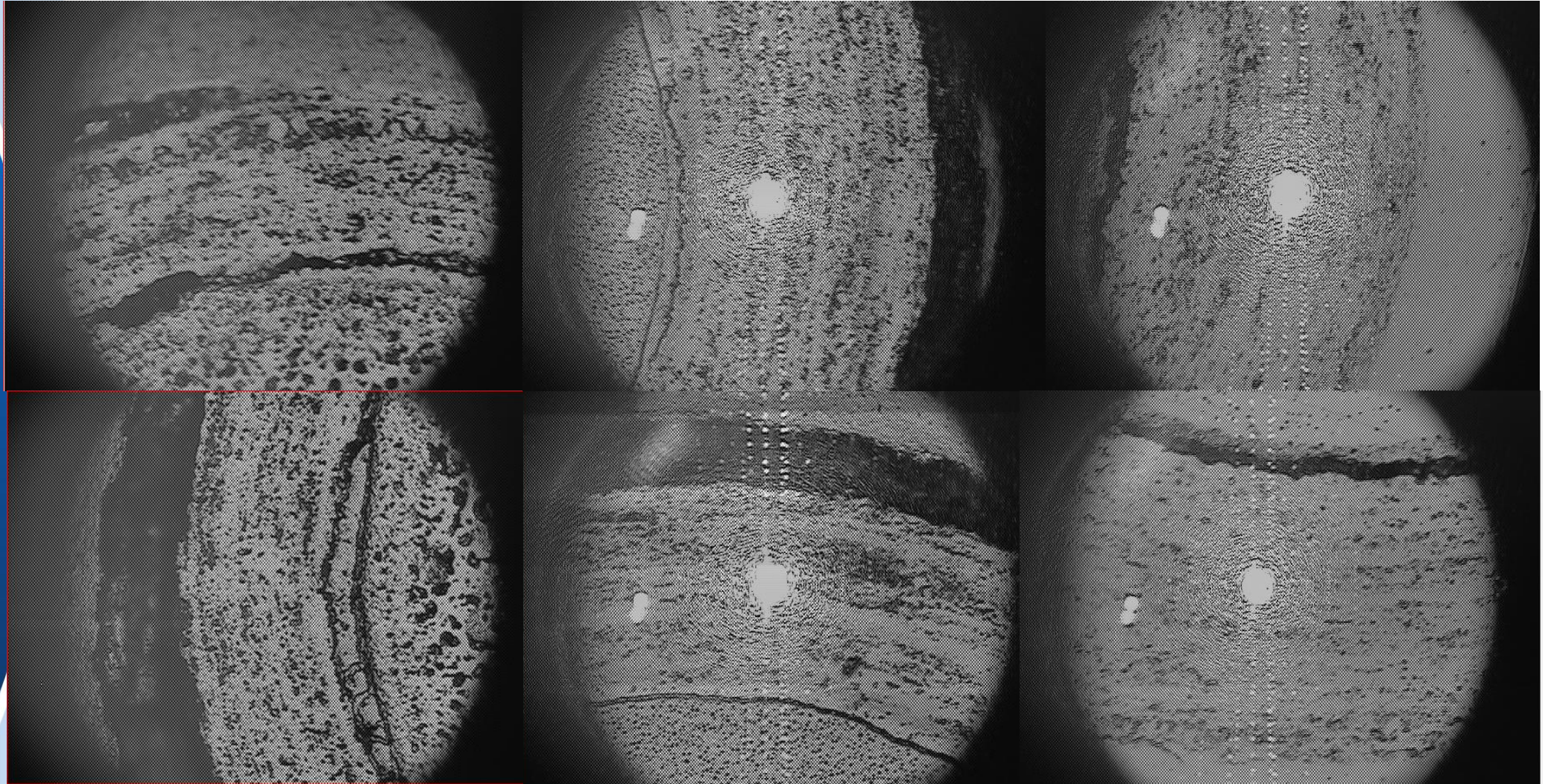
# MNT-58X Fuel Summary



# Substrate surface was not always ideal



# Buffer Layering By Compact



From left to right, 1216°C TAVA, 1078°C TAVA, and as fabricated fresh particles

# EMT of TRISO Compacts using PARFUME by Folsome et al. [9]

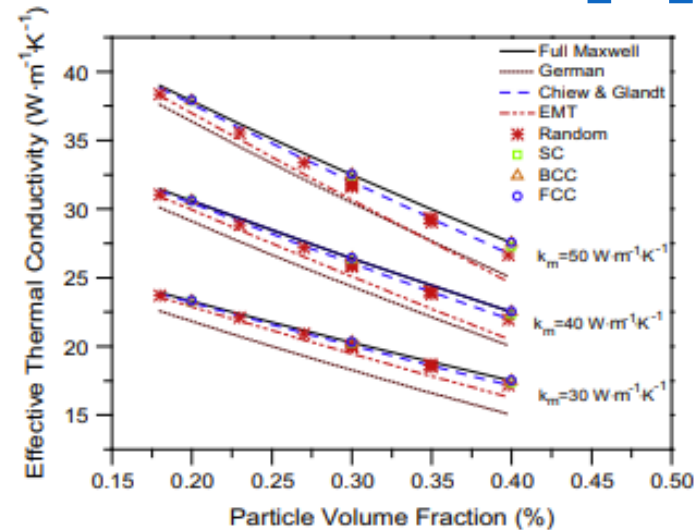


Fig. 5. FEA results for the ETC of the fuel compact for multiple matrix thermal conductivities ( $k_m$ ) compared to analytical ETC models as a function of particle-volume fraction. Particle thermal conductivity is taken as  $4.13 \text{ W m}^{-1} \text{ K}^{-1}$ .

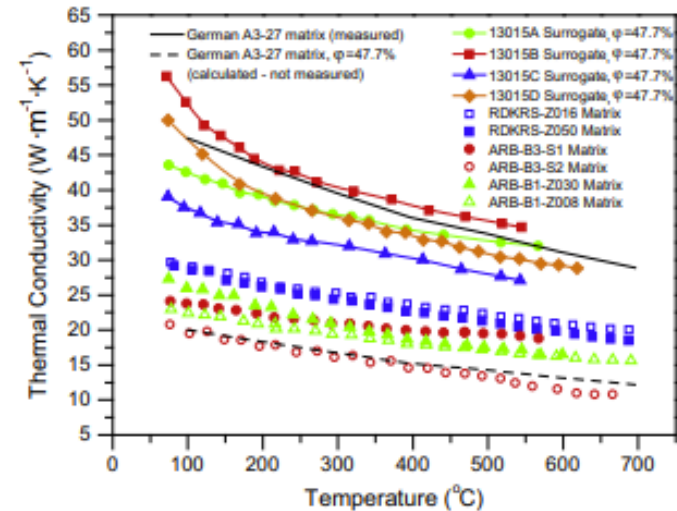


Fig. 6. Measured thermal conductivity results of matrix-only and surrogate samples plotted with legacy German data. Sample information can be found in Section 3.2.

- Developed an EMT of the TRISO compacts based on values from PARFUME
- Predicted that addition of relatively insulating particles ( $\sim 4 \text{ W/m}\cdot\text{K}$ ) into the matrix would reduce the ETC of the bulk
- Experimentation proved the opposite. The addition of the particles lead to a higher thermal conductivity of the bulk compact. Possible causes:
  - The disordered matrix becomes more ordered with the addition of particles, leading to a higher thermal conductivity
  - The particle layers are treated as very insulating, and the particle thermal conductivity would need to be ( $\sim 100 \text{ W/m}\cdot\text{K}$ ) to explain experimental results
- Likely some combination of local reordering of the matrix around the particles, and higher layer thermal conductivity



# Stempien et al. findings on UCO fuel

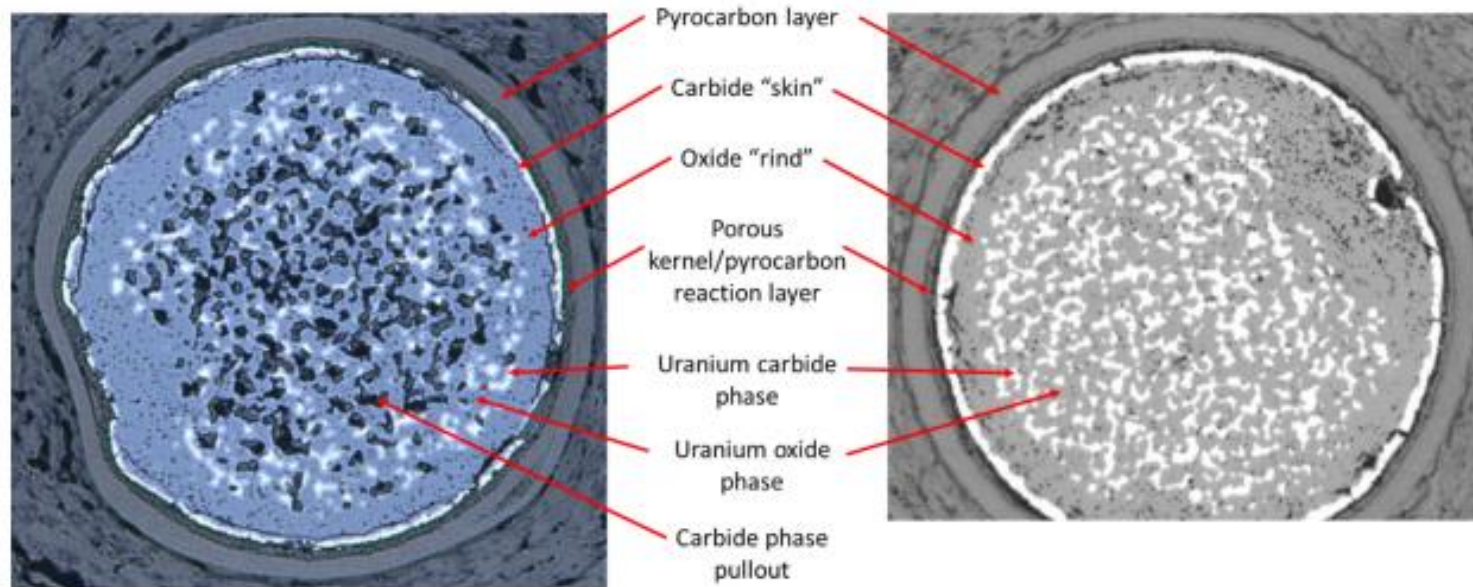


Figure 9. Cross-section of unirradiated DTF particle "1" from MNT78A (see Figure 8) in this work (left) and from work on a different, unirradiated compact in Hunn et al. 2011 Figure 1-13 (right).

- Fuel kernel forms a distinct uranium carbide phase and a uranium dioxide phase
- Edge of fuel kernel forms an oxide rich fuel region
- Layer of carbide forms between buffer and fuel kernel